Analysis of the Cromwell, Minnesota Well 4 (593593) Aquifer Test

CONDUCTED ON MAY 24, 2017
CONFINED QUATERNARY GLACIAL-FLUVIAL SAND AQUIFER

DEPARTMENT OF HEALTH

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Data Collection and Analysis

The constant-rate aquifer test performed at Cromwell 4 (593593) was conducted as described below. The test results are summarized in Table 1. The specifics of test location, scope, and timing are presented in Table 2, Table 3, and Table 4. Data were analyzed using standard methods cited in references. Individual analyses are presented the Figures 1-25 and are summarized in Table 5 and Table 6. Figures 26-44 include maps, comparison of manual and electronic data, and any other test documentation. Records of well construction are contained in Figures 45-54.

Description

Purpose of Test

The test of Cromwell 4 was conducted by the Minnesota Department of Health (MDH) Source Water Protection Unit as a small part of a longer-term project led by the United States Geological Survey (USGS). The overall purpose of the study is to assess the rates of groundwater recharge through low-conductivity glacial sediments at various sites in Minnesota.

Specific to Cromwell, eight observation wells were installed by the USGS in 2015. Water elevations were recorded on a one-hour interval in five of these wells for approximately one-year. The USGS had completed its data collection and was preparing to seal the observation wells. Prior to sealing the wells, notification was provided to the partner agencies relative to the completion of the work. At that time, staff in the Source Water Protection Unit recognized that this configuration of observation wells is nearly ideal for conducting a short-term constant-rate aquifer test that is designed to estimate vertical groundwater flow induced by pumping. Therefore prior to sealing the wells, MDH proposed to conduct tests that would complement the USGS data collection efforts.

Well Inventory

The well records are presented in Figures 45-54 and the well construction is summarized in Table 2. Detailed site plans are shown in Figure 26 and Figure 27.

Hydrogeologic Setting

These records were used to assess the hydrogeologic setting and identify the appropriate conceptual model for data analysis. A schematic section through the test site is shown on Figure 28 to illustrate the three layers that comprise the flow system; water table, aquitard, aquifer, and the construction of wells within these layers.

Other Interfering Wells

No other high capacity wells exist in the area to cause interference.

Test Setup

The USGS provided the pressure transducers and data loggers used for long-term monitoring, re-programmed to a one-minute interval. MDH hydrologists, Tracy Lund and Justin Blum, traveled to Cromwell on May 18, 2017 to assess site conditions and re-install the transducers to collect background water level and barometric data. At that time, the flowmeter-totalizer had been removed for cleaning and calibration. Mr. Tom Johnson, the water operator, indicated that the flowmeter would be returned to service shortly and the test was tentatively scheduled to begin on May 23, 2017.

Access to Cromwell 3 (519761) is restricted and the only means to measure the water level is via a bubbler-line. A transducer could be placed in Cromwell 4 to monitor water levels. A prior test of Cromwell 3 was conducted by the MDH in 2001. The location of the obwell nests relative to the PWS wells is slightly closer to Cromwell 4 than 3. The obwells constructed in the till are within 60 feet of Well 4 and are therefore more likely to respond to pumping. Because of these factors; access to the wells, prior tests, and the relative distance of the well nests, caused Cromwell 4 to be preferred for testing.

After the flowmeter was reinstalled, MDH staff mobilized for the test on May 24, 2017, arriving on-site at 10:00. The flow monitoring equipment and pump controls were inspected with the operator. Discussions with the operator indicated that the system demand is much smaller than the capacity of the well and water will have to be wasted during the 24-hour pumping phase. He considered putting a discharge control on one of the hydrants to drain the excess but opted to let the tower fill and overflow to the established drain. This presented no flooding or erosion hazard and did not require monitoring for concerns of public safety.

An MDH pressure transducer was installed in Cromwell 4; programmed to a 20 second interval, and scheduled to begin data collection 5/24/2017 at 12:00. Static levels were collected from all accessible wells prior to beginning the test. A transducer (in-line with a compressor) was attached to the Cromwell Well 3 bubbler-line to attempt to collect water levels.

Weather Conditions

Conditions were cool and rainy during background data collection. No appreciable precipitation occurred during pumping and recovery.

Discharge Monitoring

The totalizing flow meter was read manually to document the pumping rate. The operator flushed hydrants between 12:30 and 15:00, early in the pumping phase, putting some of the excess water to productive use.

Data Collection

The pump was started at 12:10:04 on 5/24/2017 by hand control. The compressor/transducer setup on Well 3 did not collect usable data. Water levels were collected manually from the accessible wells and data were downloaded to check the operation of the transducers.

It was found that the transducer in well USGS 2-E (773064) was set too deep in the well and did not collect usable data during background and early pumping. The submergence of the transducer was adjusted and a static collected at 15:30. Data collected after about 280

minutes of pumping (~18:00 on 5/24/2017) are valid. The transducers in all other observation wells appeared to functioning properly.

In the morning of 5/25/2017 distances from the pumped well to the observation wells and other features visible on aerial photos were measured with fiberglass tape. Data were downloaded from the transducers prior to end of pumping/start of recovery. Recovery began at 12:25:00 5/25/2017.

During the recovery period, over the Memorial Day weekend, the water operator agreed to manipulate the pump controls is such a way that Well 4 would not be pumped and Well 3 would be used to meet demand. Normal operation is to alternate the wells, accomplished by an automatic switch in the pump controls. Bypass of the switch provided data from short-term pumping of Well 3 to compare to that from the test of Well 4, just completed, see test 2613.

Data were downloaded on 5/30/2017 and water levels measured. The recovery-phase data from USGS 1-A was lost during the download process. Also, inspection of the data from Well 4 showed that the hydrant flushing caused anomalous changes in water level in the early part of the pumping-phase. Because of these problems, it was decided to perform a second, short-term constant-rate test, of Well 4 to attempt to collect additional early-time data from the pumped well and USGS 1-A. This test was run the same way as the earlier constant-rate test but for an abbreviated pumping period (345 minutes) with an overnight recovery. The final water levels were measured on 5/31/2017 and the equipment removed from the wells. Results of this short-term test are described in a separate document, see test 2619.

Qualitative Aquifer Hydraulic Response

Detailed site plans are shown in Figure 26 and Figure 27, identifying the wells and distances between the wells. A schematic cross section is provided for visual context of the test conditions, Figure 28. Comparison of manual and transducer data are shown Figure 29 through Figure 37. All but one well showed a response to pumping. USGS 2-A, constructed in the water table aquifer showed no response, as expected. The groundwater gradient is upward under 'static conditions,' including typical pumping to meet the system demand, Figure 38. The ambient difference in water elevation across the till at the well site is approximately 8.4 feet. Comparisons of water elevations between wells at the nests are shown on Figure 39 and Figure 40. From these comparisons, the more intensive pumping of this constant-rate test temporarily reversed the gradient within a short distance from the pumped well (~10 feet) and generated a strong signal for analysis of hydraulic properties.

The water elevations appear to trend upward over the data collection period. No appreciable change in water level can be attributed to changes in barometric pressure, Figure 41. The trend of the increase in water level shown on Figure 37was removed prior to analysis.

The only truly anomalous hydraulic responses were seen in wells USGS 2-B and 2-C, Figure 34 and Figure 35, respectively. These wells showed consistent, transient, reverse water level variation with the start of pumping of either Cromwell 3 or 4; conditions under which elevations would be expected to decrease. The reverse water variation also occurred at the end of the Cromwell 4 pumping phase. The magnitude of the response was about 0.1 foot and dissipated within about twenty minutes of the change in conditions. This phenomenon has been described in the literature as a poro-elastic response, Wolf (1970). Reverse water level fluctuations are characteristic of wells constructed in materials with a low conductivity and high elasticity (clay) that are in contact with materials of high conductivity and high compressive strength (sand). This condition is rarely observed and is the first time that it has been encountered (that we are aware of) in Minnesota. Because of this poro-elastic

response, data from these wells are considered to be most representative of conditions within the till, relative to the response of other wells in this nest.

Within the aquifer itself, the simplifying assumptions of commonly used analysis techniques consider the movement of groundwater induced by pumping to be exclusively horizontal. In the case of this analysis, vertical head differences within the aquifer within 200 feet of the pumped well cannot be neglected. The pumping well is constructed with a twenty-foot screen, centered 55 feet below the top of the sand and gravel aquifer. The total thickness of the aquifer in this location is 145 feet. This type of well construction where the aquifer is screened over only a portion of the whole thickness is known as 'partially penetrating.' Because of this well construction, within small radial distances (tens of feet) from the pumped well, groundwater flow is spherical rather than horizontal; transitioning to horizontal with increasing radial distance. The rule of thumb (Hantush, 1964) for estimation of the radial distance at which this transition to horizontal flow is complete:

$$\mathrm{r_h} = 1.5 * (aquifer\ thickness) * (\frac{horizontal\ conductivity}{vertical\ conductivity})^{0.5}$$

Given the geometry of aquifer materials and well construction at this site; and, if there is no difference between horizontal and vertical hydraulic conductivity, then the minimum distance to the transition to horizontal flow is 217 feet. [In fluvial sediments, the vertical conductivity is normally smaller than the horizontal conductivity – increasing differences between these conductivities will produce a progressively larger radial distance of transition.] Both well nests are within this minimum distance and therefore the effects of partial penetration should be expected to be present.

The partially penetrating condition was verified in Aqtesolv, Figure 42, as being the result of spherical flow by the similarity of the slope of data to the diagnostic curve. A non-Theisian response was also seen by the approximate unit-slope of early-time data USGS 1-B, on a log-log plot before 200 minutes, Figure 43. The portion of the transient response before 200 minutes, dominated by spherical flow, should not be used for analysis by methods that do not incorporate partial-penetration.

An additional consideration for the analysis of aquifer properties is the decrease in conductivity at the top of a layer resulting from fluvial depositional processes. This is typically described as the 'fining upward' distribution of gain-size when looking at layers of sediment in cross-section. Because of this tendency, it is expected that the conductivity of the material at the top of the aquifer would be smaller than that at the level of the pumped-well screen or at the base of the aquifer.

This expectation is consistent with the remarkable similarity of the observed hydraulic response of USGS 1-B and 1-C, in the middle and at the base of the aquifer, Figure 43 and Figure 44. The similarity of response indicates a negligible contrast in horizontal and vertical conductivities for middle to lower parts of the aquifer. With regard to the response at the top of the aquifer, a smaller conductivity normally implies a larger drawdown. However, the drawdown at the top of the aquifer cannot be greater than that observed at USGS 1-B, at the level of the pumped-well screen within the aquifer. This represents a bounding condition on estimates of drawdown, useful to inform the analysis.

Quantitative Analysis

Typically, an aquifer test characterizes the hydraulic properties of aquifer materials and if additional information can be extracted relative to the bounding aquitards; it is generally considered a 'bonus.' However, the primary question for this project is the assessment of

the vertical movement of water in the till. Therefore, the goals of this project require a different approach.

The difference in water pressure across the aquitard drives the leakage through the till. The pressure at the top of the aquitard is well documented (USGS 2-A); but, is unknown at the base of the aquitard/top of aquifer. The uncertainty is the result of the effects of the partially-penetrating pumping well. Consequently, uncertainty in the drawdown at the boundary between the aquifer and till causes uncertainty in the leakage rate. Because of these complications, the analysis must proceed in stages and must be checked at each stage for consistency with the conceptual model of a partially penetrating well in a leaky-layered system.

The analysis process is broken into parts or steps that use different groups of wells to focus on how the aquifer works (conceptual models). Steps 1 through 4 lead to an assessment of representative (bulk) properties of the aquifer and aquitard. Step 5 is the analysis by the Neuman-Witherspoon method that emphasizes the impact of lithological variation within the till on hydraulic response and estimated aquifer properties. These different views of the data and how the aquifer works must converge to a set of relatively consistent aquifer properties for there to be some confidence in the test results.

Transient-Horizontal Flow

The hydraulics of a partially-penetrating pumping well has been developed in the literature with several published solutions. Some of these solutions have been implemented in the commercial aquifer test analysis software, Aqtesolv, (Duffield, 2007). This tool was used to simulate the aquifer response by a method that includes partial-penetration and leakage, a solution referenced to Hantush-Jacob (1955).

The base data set for the simulation included data from the pumped well and USGS 1-B. The goal of these simulations was to solve for reasonable aquifer properties and predict the drawdowns at the nest locations at the base of the till/top of the aquifer. The drawdown was simulated as 'virtual piezometers' at these locations. The solutions from these analyses uniformly produced very large transmissivity, small storativity, and large leakage factor, Figure 1. Well USGS 1-C was included in the solution shown on Figure 2. These simulations were not judged to be realistic because drawdowns at the virtual piezometers were uniformly smaller than that predicted by the response of the USGS obwells. It was found that inclusion of data from the pumped well was forcing an inappropriate solution.

The analysis based on data from only USGS 1-B is considered to be most reasonable to begin this process, Figure 3. This analysis produced aquifer properties that are in the reasonable range for transmissivity and storativity; including a vertical/horizontal conductivity ratio of ~0.5 and a leakage factor of ~360 feet (1/B = 2.8e-3). As the focus of this analysis is the properties of the till, the conductivity ratio and leakage factor are useful to simulate the effects of pumping at the base of the till at Nests 1 and 2. The transmissivity at the base of the till is expected to be in the range of 2,200 ft^2/day. And, based on this leakage factor, the X-axis intercept (semi-log plot of distance drawdown) is expected to be in the range of 400 feet (L * 1.12). Based on the aquifer properties from Figure 3, the drawdowns at the virtual piezometers are modeled to be in the range of 5 and 3 feet at Nests 2 and 1, respectively.

Steady-State Horizontal Flow

A distance-drawdown plot is used for the combined transient (Cooper-Jacob [1946]) and steady-state analysis (Hantush-Jacob [1955]), Figure 1 through Figure 4. This view of the aquifer response, based only on Cromwell 4 and USGS 1-B, produces a large transmissivity

and large leakage factor (very low rate of leakage). The quantities are incorrect because the conceptual model is incomplete (no partial-penetration or anisotropy). The utility of this plot is that the slope of this regression defines the maximum drawdown in the aquifer system at any radial distance. Therefore, the estimated drawdown at Nest 2 cannot be greater than ~5.3 feet.

Steady-State Vertical Flow

At Cromwell, the till is quite leaky and all observation wells constructed within the till clearly responded to pumping. The number of observation wells at Nest 2 provides the most direct estimate of water pressure at the base of the till/top of the aquifer. The configuration of the well nest is analogous to test column of granular material in the laboratory where observation wells act as individual pitot tubes.

A linear regression of the observed drawdowns from the Nest 2 observation wells, after 1450 minutes of pumping and projected to 10,000 minutes, Figure 5. These values were used to estimate the possible drawdown at the base of the till, ranging from 4.8 to 5.8 feet, Figure 6. Lithological differences between USGS 2-D and USGS 2-E are the cause for this large range. The regressions that followed the trend of wells USGS 2-B and 2-C were favored because of reasons discussed above. Additionally, there are physical limits on the drawdown at the base of the till, as discussed above. The range of drawdown at Nest 2 from this analysis is consistent with that from the steady-state horizontal flow of approximately 5.3 feet.

The drawdown at Nest 1 can only be roughly estimated because a single observation well was constructed in the till, USGS 1-A. A similar regression to that described above was performed to estimate the drawdown at the base of the till at this Nest. Figure 7 shows these regressions at, 2.0 and 2.95 feet at 1450 minutes and 10,000 minutes, respectively. This is also consistent with the constraints on drawdown from Figure 4.

Steady-State Leakage Caused by Pumping

The consistency of these estimates was checked on a semi-log plot of distance-drawdown by comparing the slopes and X-axis intercepts, Figure 8 and Figure 9. These possible solutions produce a similar point of zero drawdown at 400 to 500 feet and reasonable transmissivities for aquifer materials at the base of the till. The storativity from these solutions is not valid because of the effects of partial penetration; however, these large values for storativity are reasonable with respect to the time that it takes for the response to pumping to propagate to the base of the till.

The leakage factor is essential for calculating the vertical conductivity of the till in combination with other parameters: transmissivity and aquitard thickness. Here, the notation for leakage factor, 'L' from Kruseman and de Ridder (1991) is used. The leakage factor from the steady-state Hantush-Jacob analysis is calculated as, $L = X_o / 1.12$. The equation for the vertical hydraulic resistance of the aquitard is, $c = L^2/T$ in units of days.

From these relationships, the vertical conductivity is calculated (in terms of L) as,

$k_V = b' / (L)^2 / T]$

As shown in Figure 9, the Hantush-Jacob analysis of distance-drawdown data produces,

$k_V = 130 / [(437)^2 * 2200] = 1.5$ ft/day.

Simultaneous Solution for Horizontal and Vertical Flow

The transient response of the observation wells constructed within the till can be analyzed by the Neuman-Witherspoon method. The responses at Nests 1 and 2 were analyzed separately and as a composite, Figure 11 through Figure 21.

The Nest 2 analyses, generally were consistent values for aquifer properties. The analysis of recovery data at Nest 2, Figure 17, produced the best match and results that most closely followed the analysis of USGS 1-B, Figure 3.

The Neuman-Witherspoon analyses from Nest 1, Figure 18 and Figure 19, produced a larger transmissivity and a larger vertical conductivity of the till. Figure 18 attempted to match the data from within the aquifer. The solution shown on Figure 19 was based on the single till observation well, USGS 1-A.

The composite analyses, matching all data from the obwells were lower quality matches and more variable results, Figure 20 and Figure 21.

Estimates of leakage factor from factor from the Neuman-Witherspoon analyses are reported as 1/B. This parameter is the same as the 'B' in 'r/B' from the steady-state Hantush-Jacob model, Walton (1960) normalized for radial distance. 1/B, is the inverse quantity, $L = (1/B)^{-1}$, and the vertical hydraulic resistance is expressed as, $1/c = (1/B)^2 * T$ in units of $days^{-1}$.

From these relationships, the vertical conductivity is calculated (in terms of 1/B) as,

$k_V = b' * [(1/B)^2 * T]$

As shown in Figure 17, the Neuman-Witherspoon analysis of data from Nest 2 produces,

$k_V = 130 * [(0.0017)^2 * 2300] = 0.86$ ft/day.

Heterogeneity in the properties of the till is indicated by the poor match of the response of USGS 1-E to the curves relative to the other wells in Nest 2, Figure 17. Examination of the slopes of the late-time data at the observation wells in the till shows that there is a marked similarity in the trends of USGS 1-A and USGS 2-E, Figure 22. Because of this similarity a separate Neuman-Witherspoon analysis was performed on only those wells, Figure 23. This analysis is a reasonable upper bound on the conductivity of the till, 4.1 ft/day.

Additional Analyses for Comparison to other Parts of the Dataset

Figure 24 and Figure 25 are recovery analyses for comparison to the short-term tests that were conducted after this test, see documents for tests 2613 and 2619.

Conclusion

The bulk aquifer and aquitard properties from this dataset are shown in Table 1, as derived from the analyses listed on Table 5 and Table 6. This test is a detailed examination of the properties of the till in a very small area. The large range of estimated aquifer properties result from both: the sub-set of the data to which an analysis method was applied, and natural lithological variation, particularly within the till.

The reported range of vertical conductivity of the till is from 0.85 to 4.1 ft/day. The low value, 0.85 ft/day, is from the response of wells at Nest 2, USGS 1-B, 1-C and 1-D.

However, the till contains significant heterogeneities and the vertical conductivity is significantly greater in some areas. Based on the responses at USGS 1-A and USGS 2-E, the largest credible value from this dataset is 4.1 ft/day. Because these wells are at both nests, it is likely that this analysis characterizes the till over a larger geographic extent than the analyses from the observation wells limited to Nest 2. Therefore, for modelling purposes it is unlikely that the low value is realistic and a more reasonable range of the bulk properties of the till is from 1.1 to 4.1 ft/day.

Acknowledgements

There have been few opportunities to collect this level of detailed hydraulic information for the analysis of rates of leakage through till. It is judged that this data collection effort and subsequent analysis was particularly successful, given the hydrogeologic setting and the normal challenges of adapting to field conditions. Credit for this success is due in large part to the active participation and support of Mr. Tom Johnson, water operator for the city of Cromwell. Thank you.

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Tables and Figures

Table 1. Summary of Results for Leaky Confined - Radial Porous Media Flow

Parameter	Value	Unit	Range Minimum	Range Maximum	+/- % variation
Top Stratigraphic Elev.	1152	feet (MSL)			
Bottom Stratigraphic Elev.	1007	feet (MSL)			
Transmissivity (T)	4,400	ft^2/day	1,000	5,700	
Aquifer Thickness (b)	145	feet	145	175	
Hydraulic Conductivity (k)	30	ft/day			
Ratio Vertical/Horizontal k[1]	0.5	0.00 %			
Primary Porosity (e_p)	0.25	0.00 %			
Storativity (S)	2.0e-4	dimensionless	1.0e-4	4.0e-4	
Characteristic Leakage (L)	500	feet	330	2610	
Hydraulic Resistance (c)	114	days	50	220	
Thickness of till (b')	130	feet			
Hydraulic Conductivity of till (k_v)	1.1	ft/day	0.8	4.1	

[1] Conductivity decreases to ~15 ft/day at top of aquifer (transmissivity, ~2,200 ft2/day)

Table 2. Aquifer Test Information

Information Type	Information Recorded
Aquifer Test Number	2612
Test Location	Cromwell 4 (593593)
Well Owner	City of Cromwell
Test Conducted By	MDH - T. Lund and J. Blum
Aquifer	QBAA
Confined / Unconfined	Confined
Date/Time Monitoring Start	05/18/2017 11:40
Date/Time Pump off Before Test	5/23/2017 4:31
Date/Time Pumping Start	5/24/2017 12:10:04
Date/Time Recovery Start	5/25/2017 12:25:00
Date/Time Test Finish	5/31/2017 11:00
Pumping time (minutes)	1454.93
Totalizer – end reading	106059750
Totalizer – start reading	105817400
Total volume (gallons)	242350 gallons
Nominal Flow Rate	167 (gallons per minute)
Number of Observation Wells	8 (see Table 3)

Table 3. Well Information

Well Name (Unique Number)	Easting Location, X[2] (meter)	Northing Location, Y[2] (meter)	Radial Distance (feet)	Ground Surface Elevation, GSE[3] (feet, MSL)	Measuring Point Description GSE+(stick-up) (feet, MSL)	Open Interval Top (feet, MSL)	Open Interval Bottom (feet, MSL)	Aquifer
Cromwell 4 (593593)	28.9	44.2	0.4	1328	~1329	1118	1098	QBAA
Cromwell 3 (519761)	62.5	45.3	112[4]	1328	~1330	1148	1138	QBAA
Nest 1								Till - QBAA - Bedrock
USGS C1-A (773071)	50.0	6.4	149.5	1326.3	1328.66+	1181.7	1178.9	Till – mid
USGS C1-B (773070)	48.8	6.3	147.8	1326.3	1328.62+	1105.4	1095.8	QBAA
USGS C1-C (773069)	47.3	6.4	145.6	1326.2	1328.78+	996.7	987.1	Thompson Fm.
Nest 2								Till - QWTA
USGS C2-A (773068)	40.6	54.0	53.9	1332.3	1334.67+	1300.0	1297.3	QWTA
USGS C2-B (773067)	40.6	56.1	58.8	1332.6	1334.98+	1275.9	1273.2	Till - top
USGS C2-C (773066)	42.2	54.0	57.7	1332.3	1334.71+	1253.6	1250.9	Till – mid top
USGS C2-D (773065)	39.1	54.0	50.9	1332.1	1334.58+	1228.5	1225.9	Till – mid
USGS C2-E (773064)	39.0	56.1	56.0	1332.4	1334.81+	1206.6	1204.0	Till - deep

[2] Local Datum

[3] Vertical Datum: NAV88

[4] Distance between well center, distance between outside of casing is 111 ft.

Table 4. Data Collection[5]

Data File Name: Well Name_Unique Number	Data Logger Type, SN:	Probe Id., Range (psi)	Install 1. Static WL[6]	Install 2. XD [7]Setting	Remove 3. Static WL	Remove 4. XD Setting	Diff. Static WL (1-3)	Diff. XD Setting (4-2)
Cromwell-4_593593	Troll 500 145815	17, 30 psi	15.86	12.55	15.39	13.30	0.47	0.75
Baro_data	Hermit 3000 45333	6, 15 psia						
1-A(773071)	OTT 382933		20.49	19.89	20.11	19.53	0.38	0.36
1-B(773070)	OTT 382932		16.12	15.34	15.31	14.60	0.81	0.74
1-C(773069)	OTT 382934		16.20	15.58	15.42	14.79	0.78	0.79
2-A(773068)	OTT 382929		29.69	29.04	29.48	28.70	0.21	0.34
2-B(773067)	OTT 382935		28.78	28.14	28.46	27.79	0.32	0.35
2-C(773066)	OTT 382936		26.95	26.46	26.52	26.07	0.43	0.39
2-D(773065)	OTT 382931		23.71	22.47	23.18	22.42	0.53	0.05
2-E(773064)	OTT 382937		25.15	37.16	23.65	35.60	1.5	1.56

[5] Notes about data collection: USGS transducers/loggers installed 5/18/2017, before 12:00 on 1-minute interval. Barometer recording from 5/18/2017 11:40 on 10-minute interval. Inspected C-3 setup for logging, no access to well except by existing bubbler line. C-4 access through submersible cap, transducer installed 5/24/2017. Initial setting of transducer in USGS 2-E (773064) too deep, device did not record usable data of background and early pumping. Transducer reset on 5/24/2017 15:28. Data not recovered from USGS 1-A logger during late pumping and recovery.

[6] WL = water level below measuring point, feet.

[7] XD = pressure transducer depth below water surface, feet.

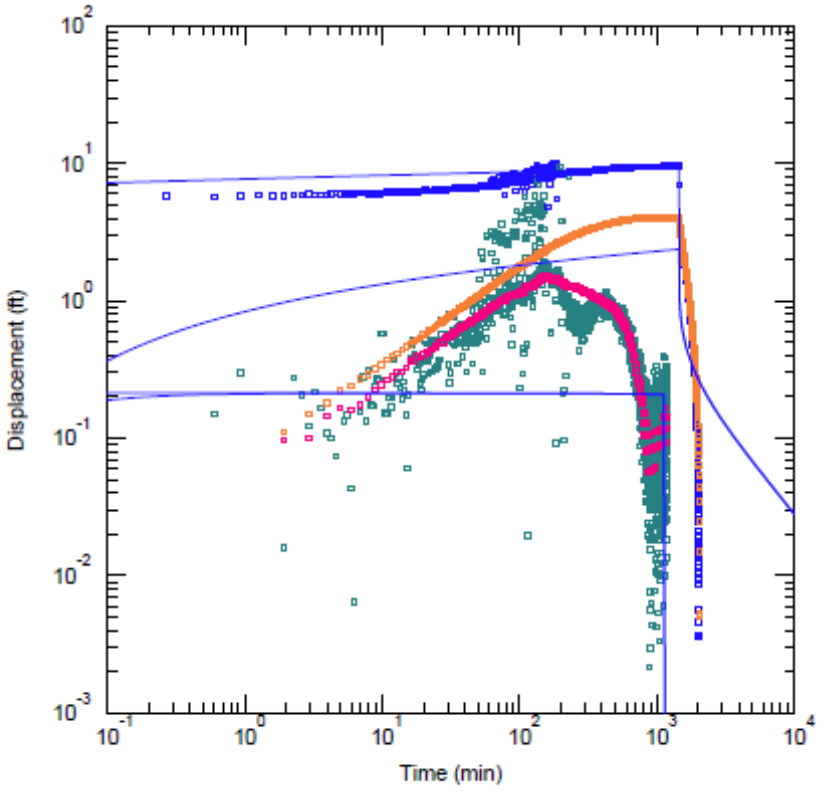
Table 5. Transient Analysis Results

Well Name (Unique Well No.)	Transmissivity, T (ft2/day)	Storativity, S (dimensionless)	Leakage Factor, L (feet)	Hydraulic Conductivity of Aquitard, kV (ft/day)	Analysis Method	Plot No. Remarks
C-4 (593593) 1-B (773070)	12,000	2.0e-5	150,000	7.0e-5	Hantush-Jacob	1. properties not credible for very leaky system
C-4 (593593) 1-B (773070) 1-C (773069)	17,000	3.5e-4	3,570	0.17	Hantush-Jacob	2. properties not credible for very leaky system
1-B (773070)	4,380	7.7e-3	330	2.6	Hantush-Jacob	3. kz/kr = 0.5, credible properties
C-4 (593593) 1-B (773070)	5,190	1.7e-4			Cooper-Jacob	4. properties not credible for very leaky system
Nest 2, all till obwell composite	2,200	5.0e-4	590	0.83	Neuman-Witherspoon	11. credible properties, consistent with plot 9, good match
2-B (770067)	2,300	3.0e-4	500	1.2	Neuman-Witherspoon	13.
2-C (770066)	2,300	5.0e-4	500	1.2	Neuman-Witherspoon	13.
2-D (770065)	1,800	1.9e-4	380	1.6	Neuman-Witherspoon	14.
2-E (770064)	2,300	5.0e-4	500	1.2	Neuman-Witherspoon	15.
Nest 2, till obwell composite, 2-D (770065) excluded from match	2700	3.0e-3	670	0.79	Neuman-Witherspoon	16.
Nest 2, till obwell composite recovery	2,300	4.0e-4	590	0.86	Neuman-Witherspoon	17. best match
C-4 (593593) 1-B (773070) 1-A (770071)	3,730	8.0e-4	1520	2.1	Neuman-Witherspoon	18.
1-A (770071)	3,550	1.2e-3	1960	1.2	Neuman-Witherspoon	19.
All till obwell composite	1,200	2.6e-3	145	7.4	Neuman-Witherspoon	20. properties not credible, too leaky
All well composite	2,790	2.9e-3	370	2.7	Neuman-Witherspoon	21.
1-A (770071) and 2-E (770064)	1590	5.0e-2	224	4.1	Neuman-Witherspoon	23. large credible k_V

Table 6. Steady-state Analysis Results

Transmissivity, T (ft^2/day)	Leakage Factor, L (feet)	Hydraulic Resistance, c (days)	Hydraulic Conductivity of Aquitard, k_v (ft/day)	Analysis Method	Plot No. Remarks
5,190	7,470	10,800	0.012	Hantush-Jacob	4. properties not credible for very leaky system
2,200	370	61	2.1	Hantush-Jacob	9. credible properties, consistent with plot 3
2,200	440	88	1.5	Hantush-Jacob	10. credible properties, consistent with plots 3 and 9

Figure 1. Solution of Aquifer Properties by Aqtesolv. Data from Cromwell 4 (593593) and USGS 1-B (773070)



WELL TEST ANALYSIS

Data Set: O:\...\00_Cromwell4.aqt
Date: 08/22/17 Time: 12:30:13

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0
1-B	140.5	0
1-C	140.4	0
2-B	0	54.8
2-C	0	53.2
2-D	0	46
2-E	0	51.7

SOLUTION

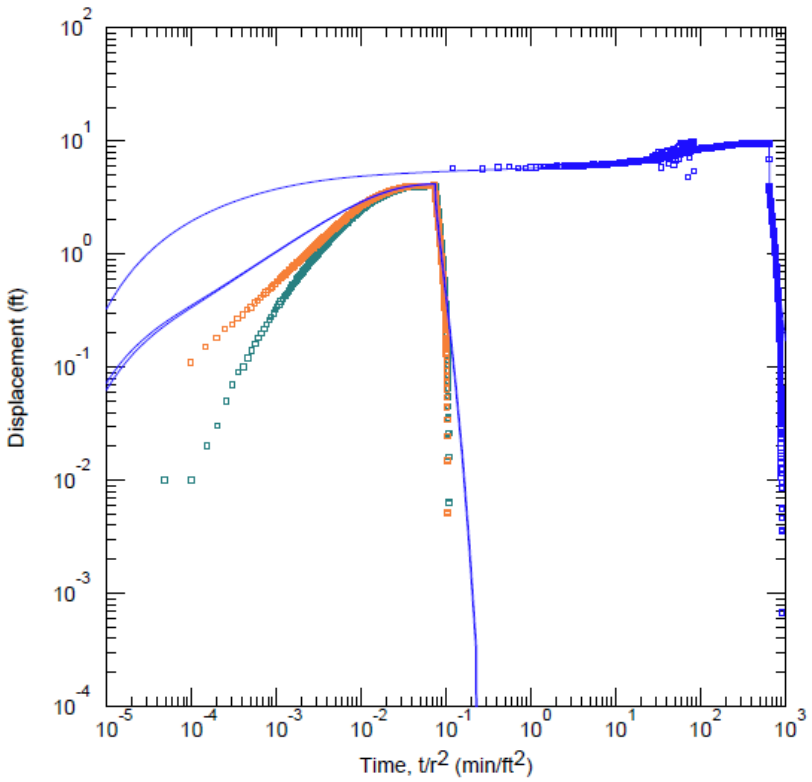
Aquifer Model: Leaky
Solution Method: Hantush-Jacob

T = 1.204E+4 ft^2/day
1/B = 6.667E-6 ft^{-1}
b = 145. ft

S = 1.974E-5
Kz/Kr = 1.

L = 149,000 feet
kv = 130 * (6.7e-6)^2 * 12,000 = 7.0e-5 ft/day

Figure 2. Solution of Aquifer Properties by Aqtesolv. Showing Data from Cromwell 4 (593593), USGS 1-B (773070) and USGS 1-C (773071)



WELL TEST ANALYSIS

Data Set: O:\...\00_Cromwell4_nest-1_composite.aqt
Date: 08/22/17 Time: 12:36:55

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0
1-C	139	0
1-B	140.5	0
1-A	142	0

SOLUTION

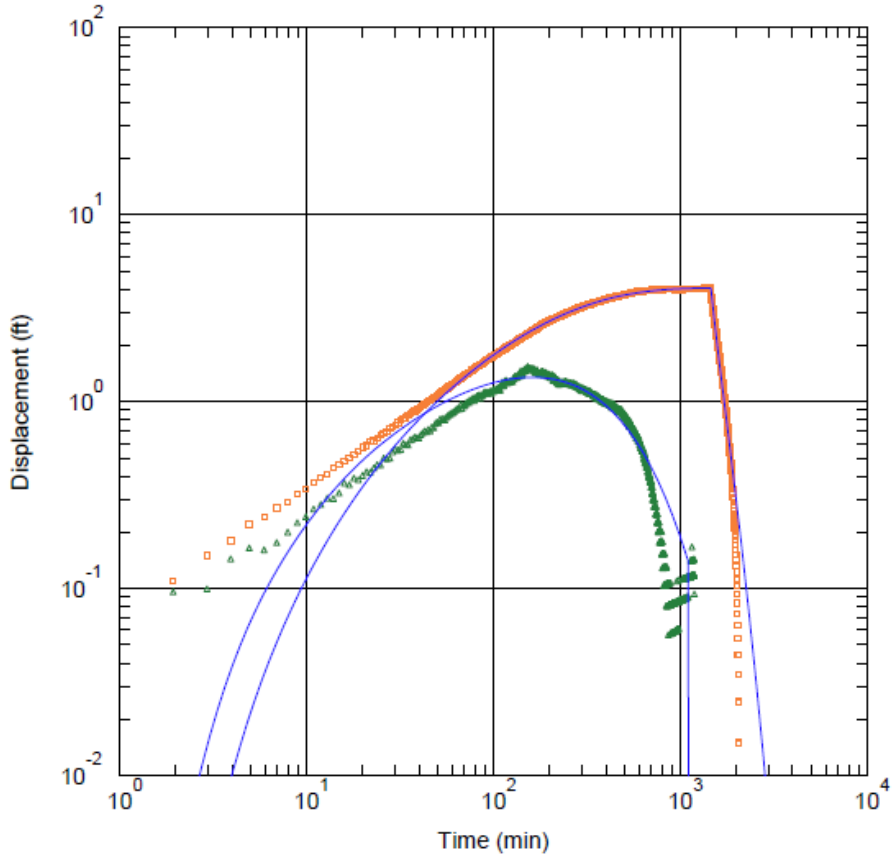
Aquifer Model: Leaky
Solution Method: Hantush-Jacob

T = 1.695E+4 ft^2/day
1/B = 0.0002804 ft^{-1}
b = 145. ft

S = 0.0003542
Kz/Kr = 0.5

L = 10,800 feet
kv = 130 * (2.8e-4)^2 * 17,000 = 0.17 ft/day

Figure 3. Solution of Aquifer Properties by Aqtesolv. Data from USGS 1-B (773070) only



WELL TEST ANALYSIS

Data Set: O:\...\01_cromwell_nest-1-B_partial.aqt
Date: 08/22/17 Time: 12:33:33

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
1-B	140.5	0

SOLUTION

Aquifer Model: Leaky
Solution Method: Hantush-Jacob

T = 4382.2 ft^2/day
r/B = 0.4231
b = 145. ft

S = 0.007766
Kz/Kr = 0.5

L = 333 Feet
k_v = 130 * (0.423/141)^2 * (4380 * 0.5) = 2.6 ft/day

Figure 4. Conventional Distance-drawdown Plot based on Cromwell 4 (593593) and USGS 1-B (773070)

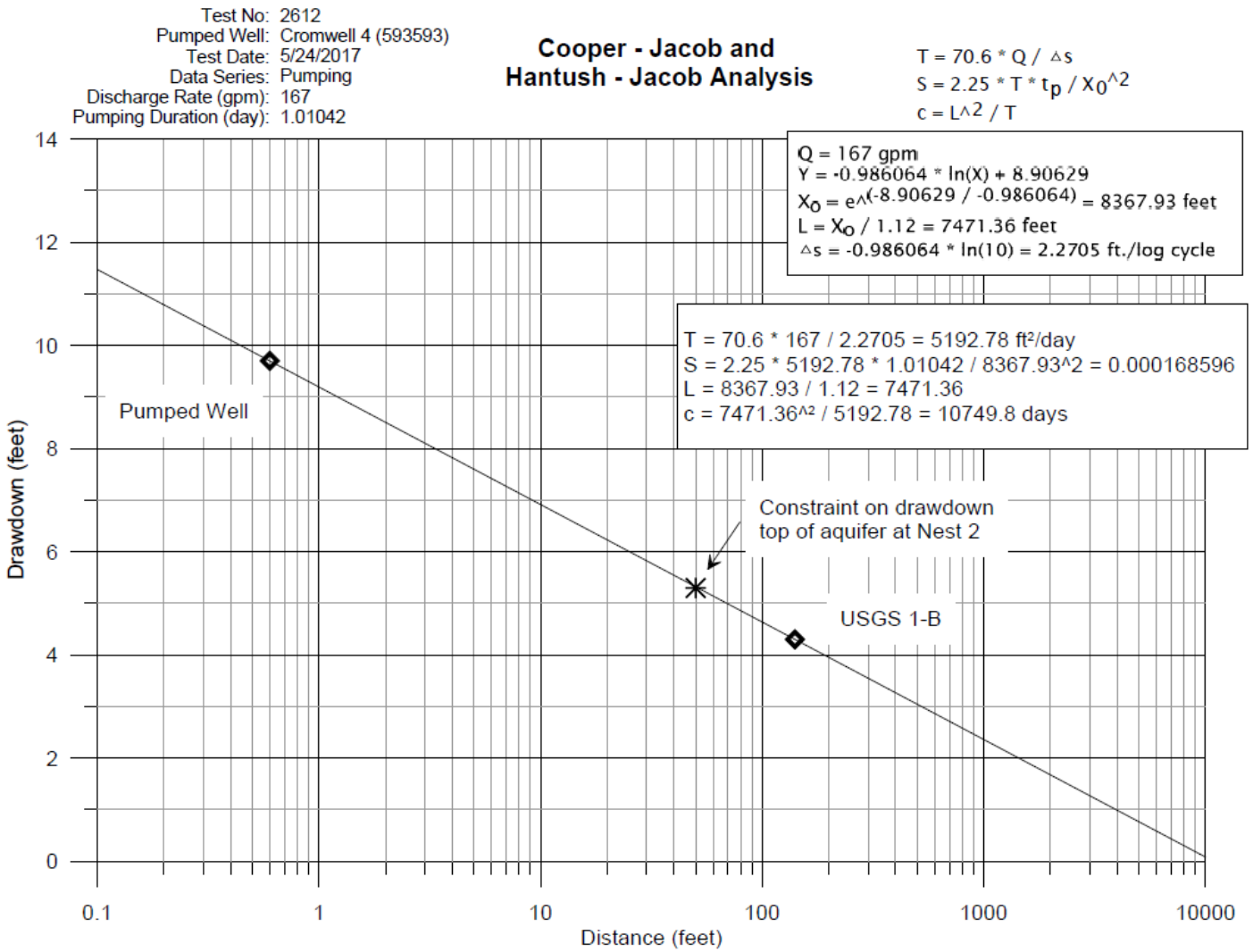


Figure 5. Drawdown at Nest 2 after 1450 minutes of pumping, projected to 10,000 minutes

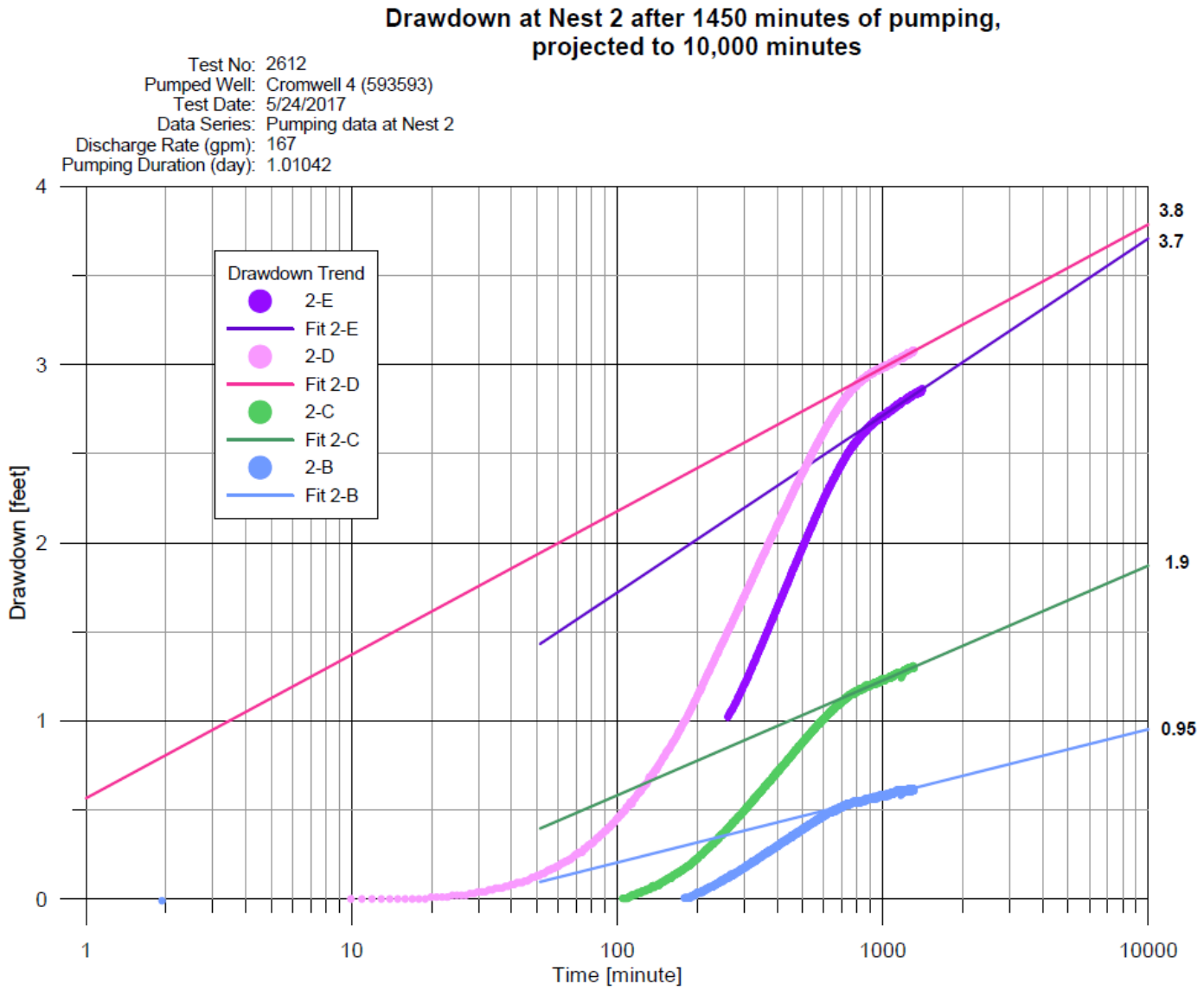


Figure 6. Groundwater Gradient at Nest 2 after 1450 Minutes of Pumping

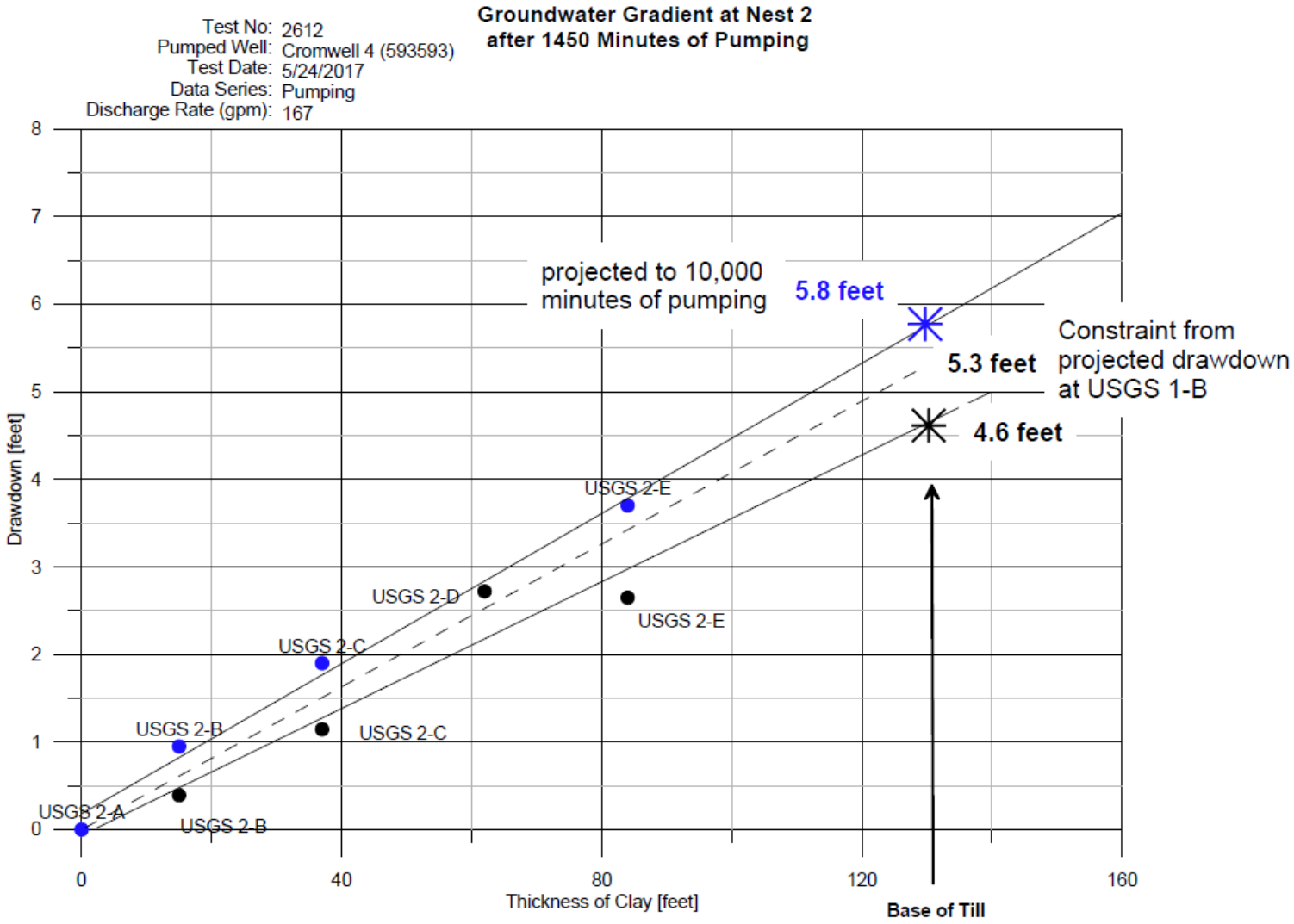


Figure 7. Drawdown at Nest 1 after 1450 minutes of pumping, projected to 10,000 minutes

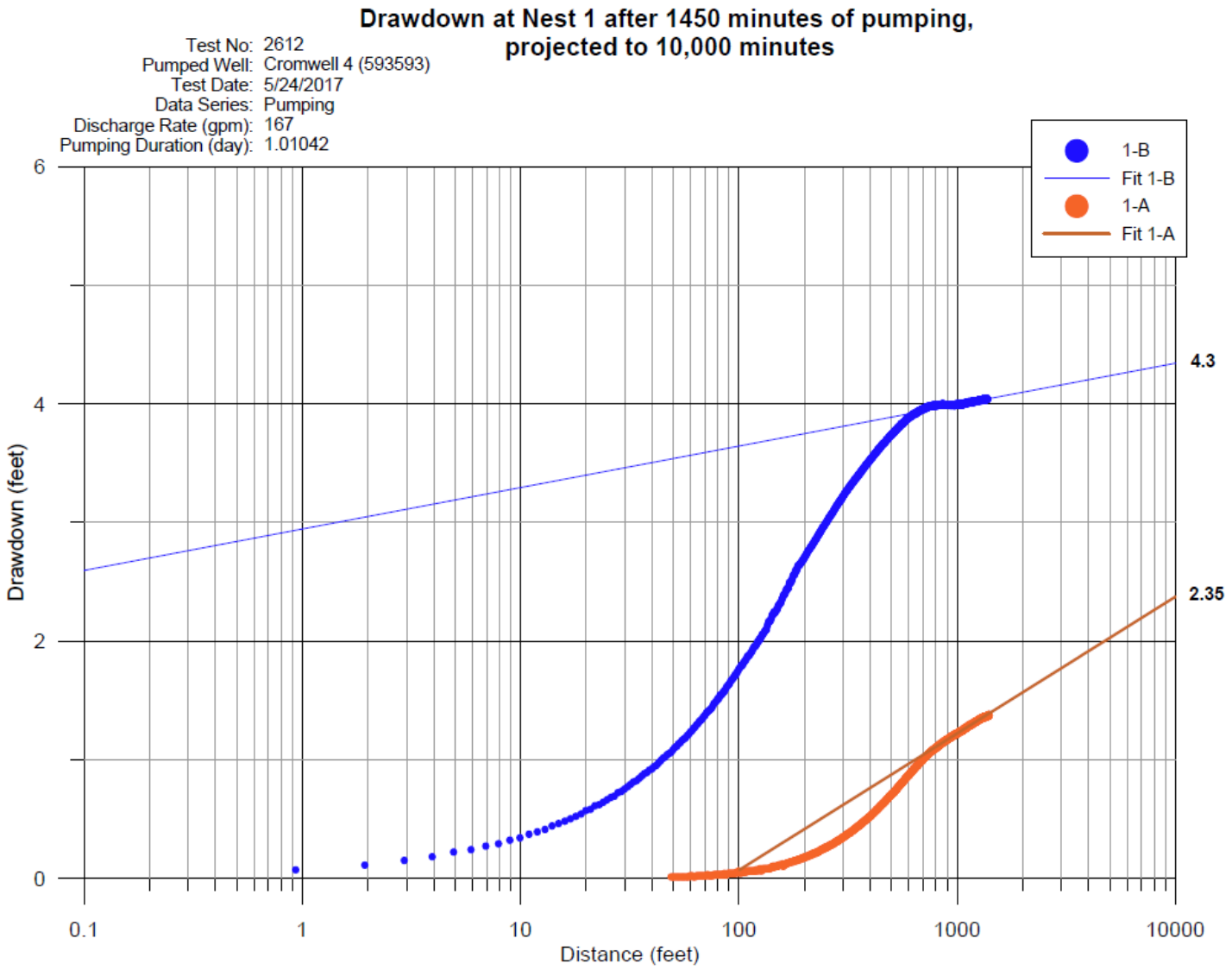


Figure 8. Groundwater Gradient at Nest 1 after 1450 Minutes of Pumping

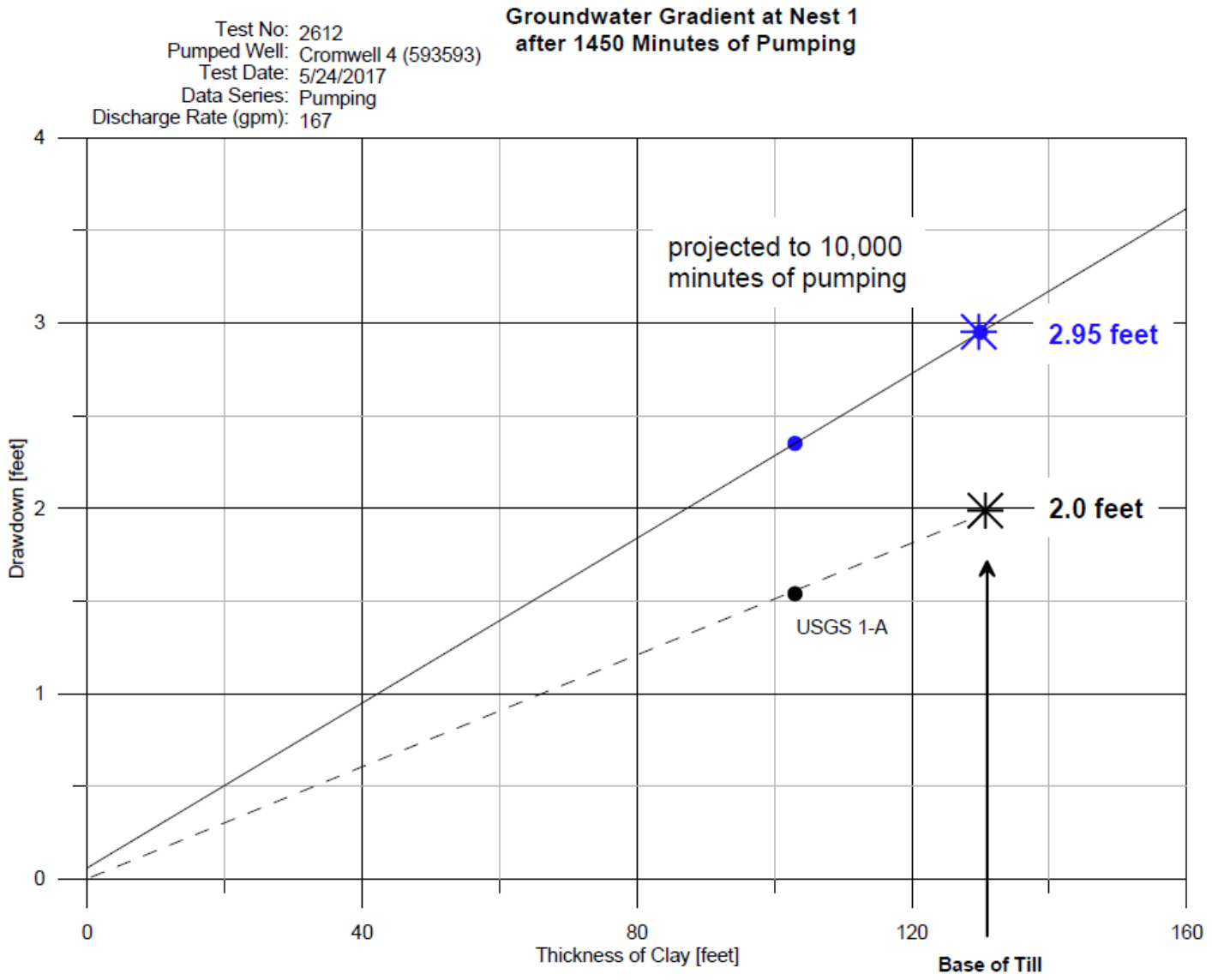


Figure 9. Comparison of Drawdowns at 1450 Minutes of Pumping at Nests 1 and 2, at Nase of Till, to that in Aquifer

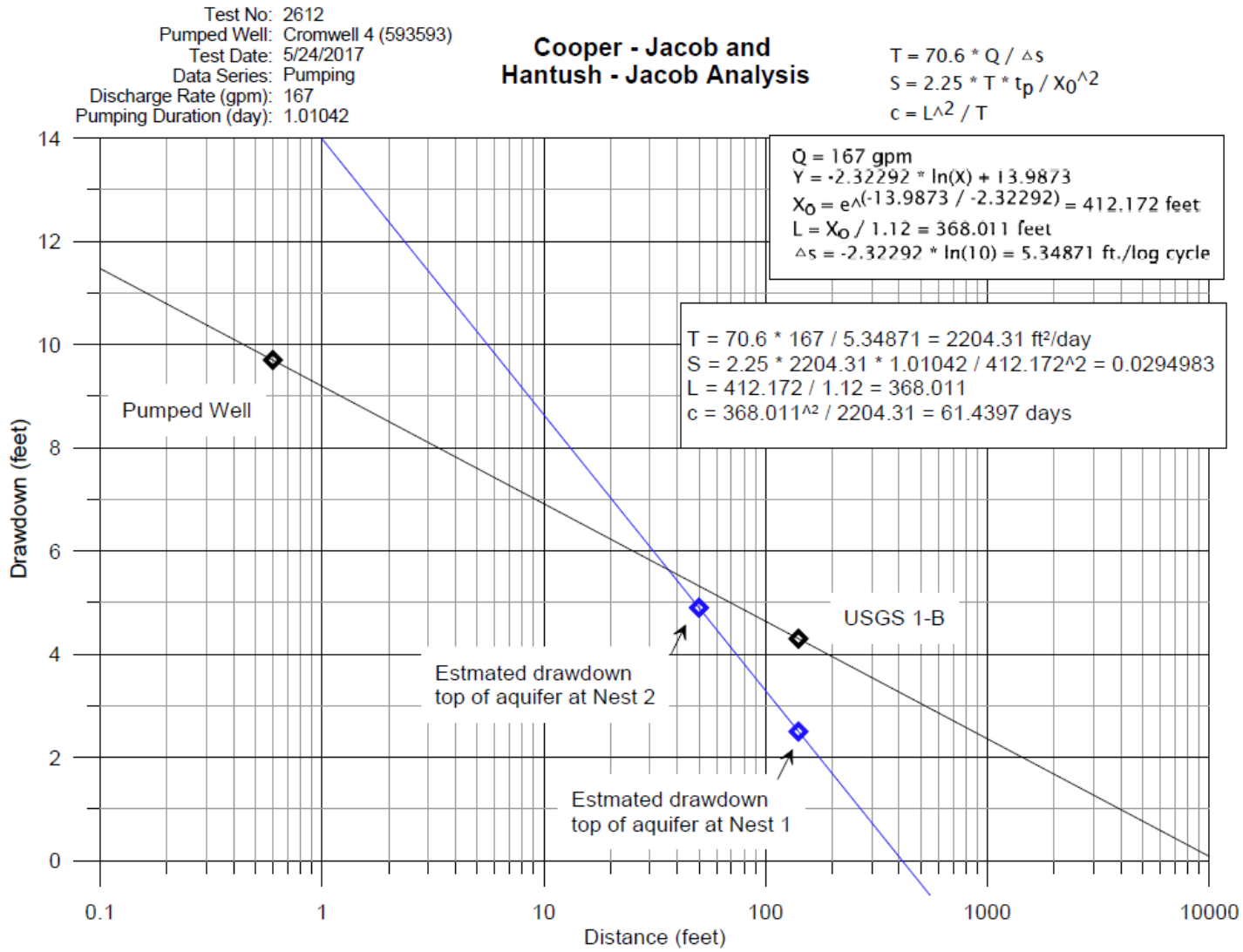


Figure 10. Comparison of Drawdowns at 10,000 Minutes of Pumping at Nests 1 and 2, at Base of Till, to that in Aquifer

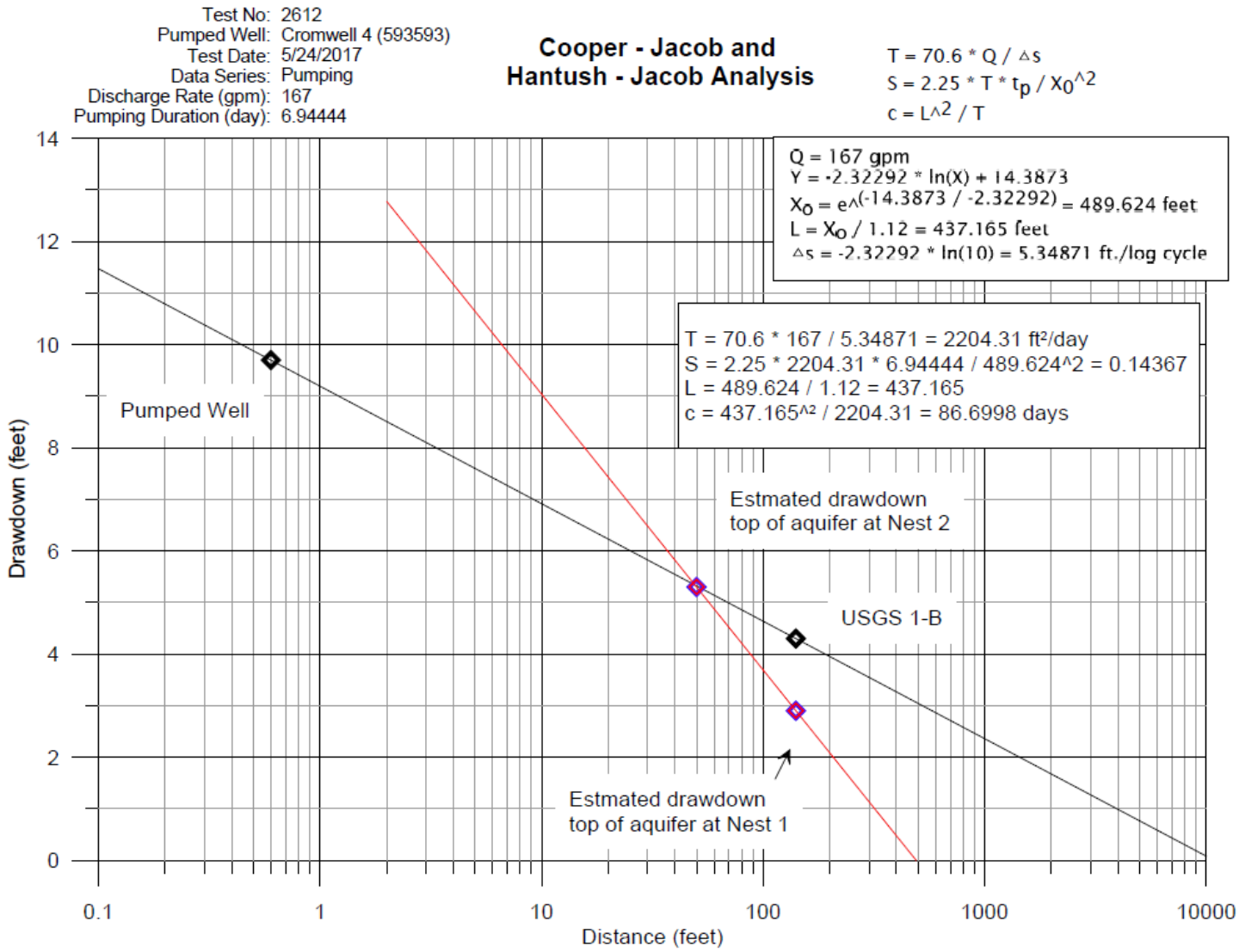
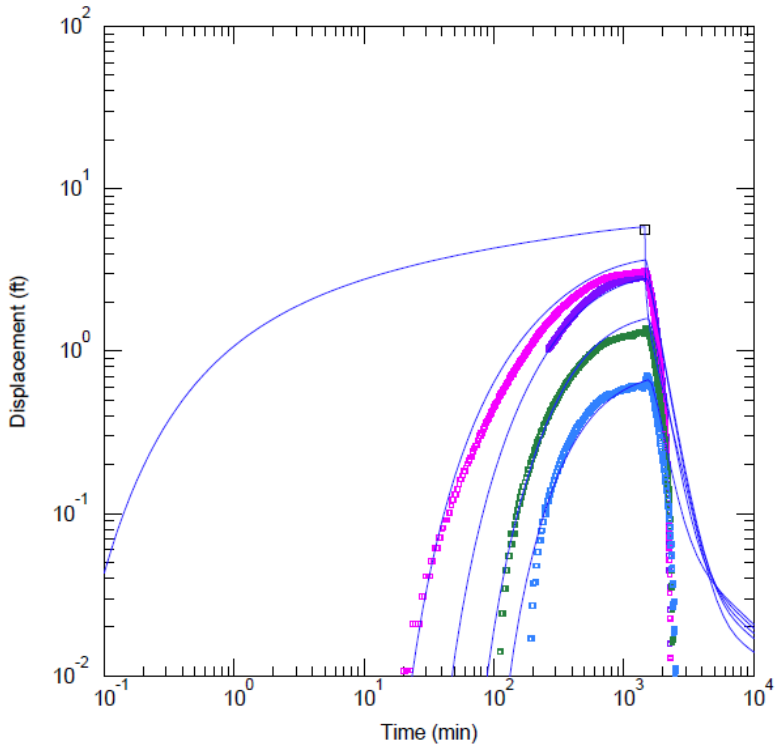


Figure 11. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B, 2-C, 2-D, and 2-E



WELL TEST ANALYSIS

Data Set: O:\...\11_cromwell_nest-2_neuman.aqt
Date: 08/22/17 Time: 15:08:21

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-E	51.7	0
USGS 2-D	46	0
USGS 2-C	53.2	0
USGS 2-B	54.8	0

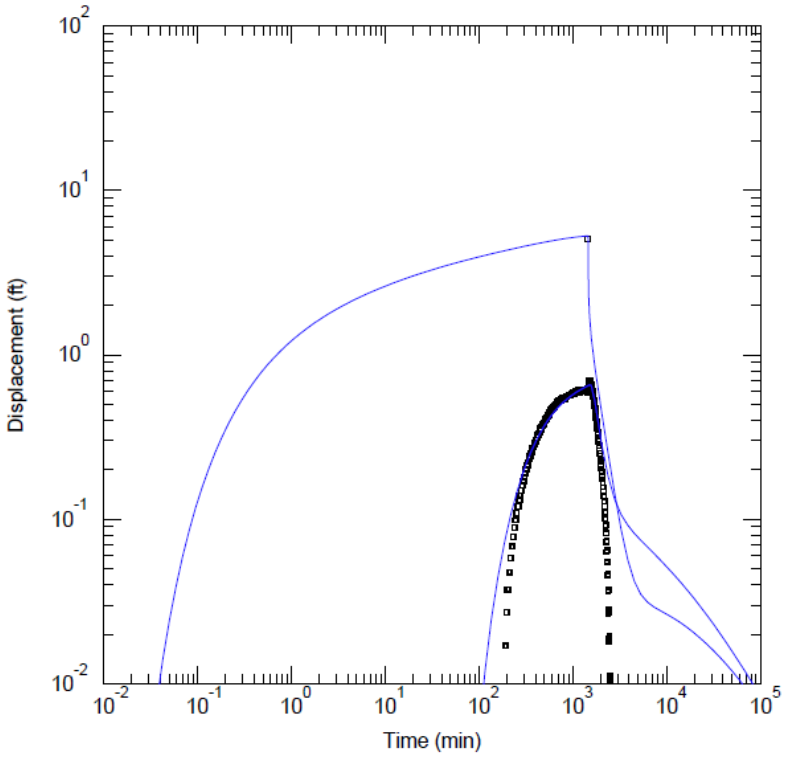
SOLUTION

Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 2200. ft^2/day
1/B = 0.0017 ft^{-1}
T2 = 10000. ft^2/day
S = 0.0005
ß/r = 0.0021 ft^{-1}
S2 = 0.25

L = 590 feet
kv = 130 * (0.0017)^2 * 2200 = 0.83 ft/day

Figure 12. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B only



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-2_neuman_2B.aqt
Date: 08/23/17 Time: 11:22:17

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-B	54.8	0

SOLUTION

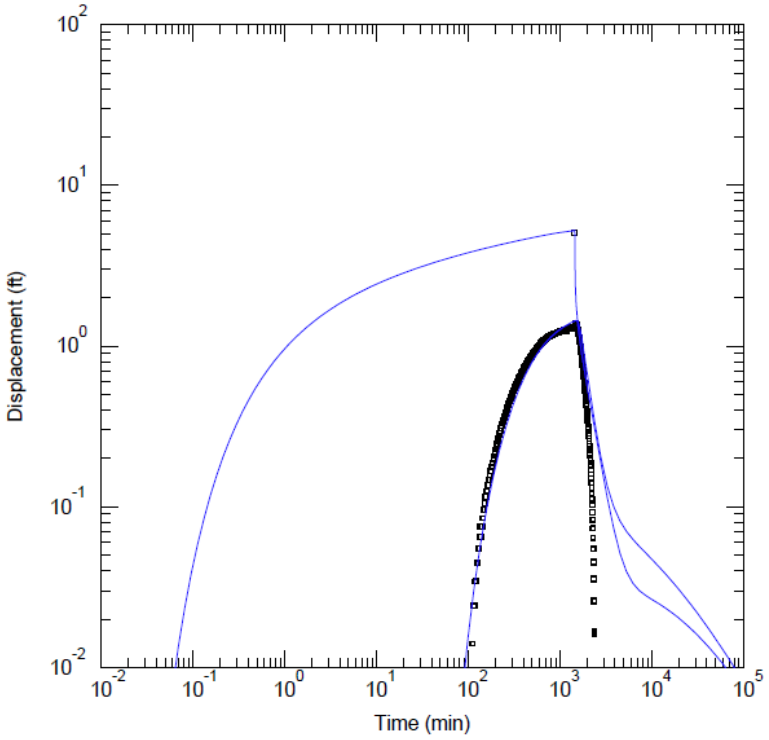
Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 2300. ft^2/day
1/B = 0.002 ft^{-1}
T2 = 2000. ft^2/day

S = 0.0003
ß/r = 0.0035 ft^{-1}
S2 = 0.25

L = 500
kv = 130 * (0.002)^2 * 2300 = 1.2 ft/day

Figure 13. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B only



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-2_neuman_2C.aqt
Date: 08/23/17 Time: 11:23:18

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-C	53.2	0

SOLUTION

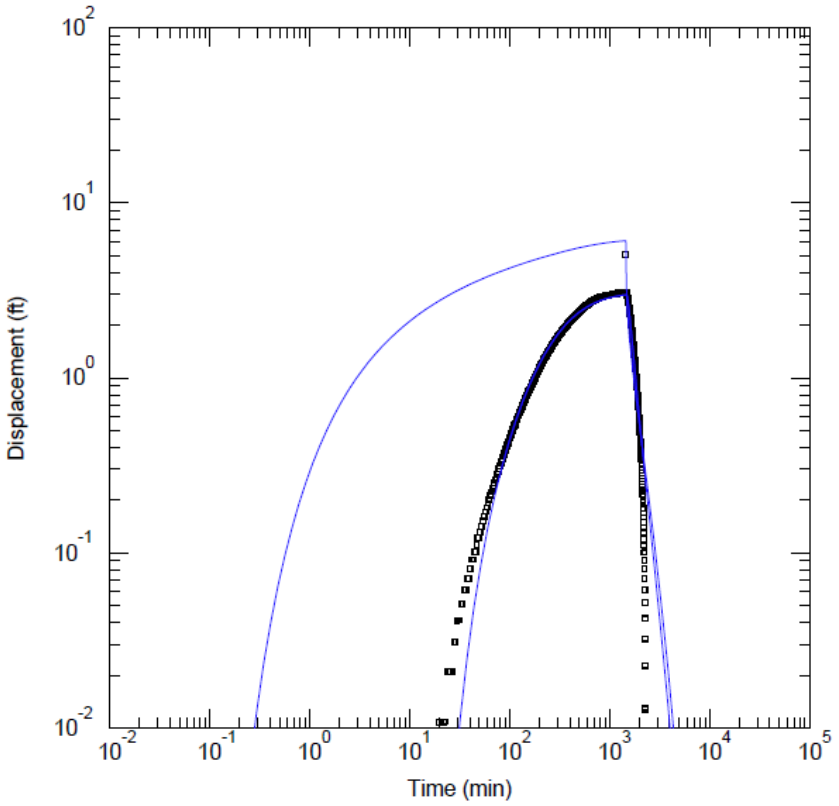
Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 2300. ft^2/day
1/B = 0.002 ft^{-1}
T2 = 2000. ft^2/day

S = 0.0005
ß/r = 0.003 ft^{-1}
S2 = 0.25

L = 500 Feet
k_v = 130 * (0.002)^2 * 2300 = 1.2 ft/day

Figure 14. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-C only



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-2_neuman_2D.aqt
Date: 08/23/17 Time: 11:24:59

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-D	46	0

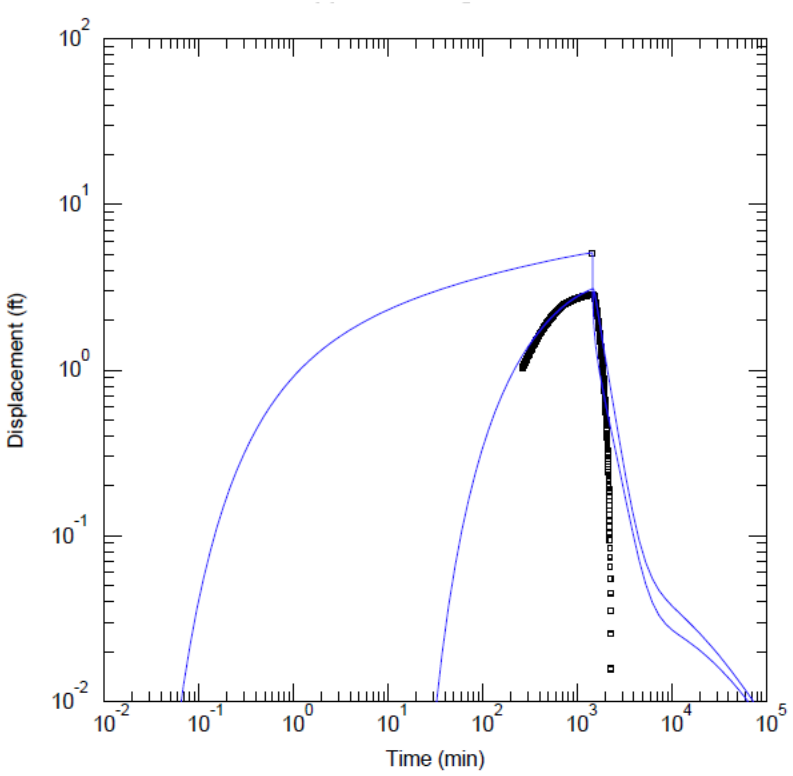
SOLUTION

Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 1800. ft^2/day
1/B = 0.002588 ft^{-1}
T2 = 1.44E+8 ft^2/day
S = 0.001862
ß/r = 0.001745 ft^{-1}
S2 = 1.

L = 380 feet
kv = 130 * (0.00259)^2 * 1800 = 1.6 ft/day

Figure 15. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-D only



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-2_neuman_2E.aqt
Date: 08/23/17 Time: 11:26:03

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-E	51.7	0

SOLUTION

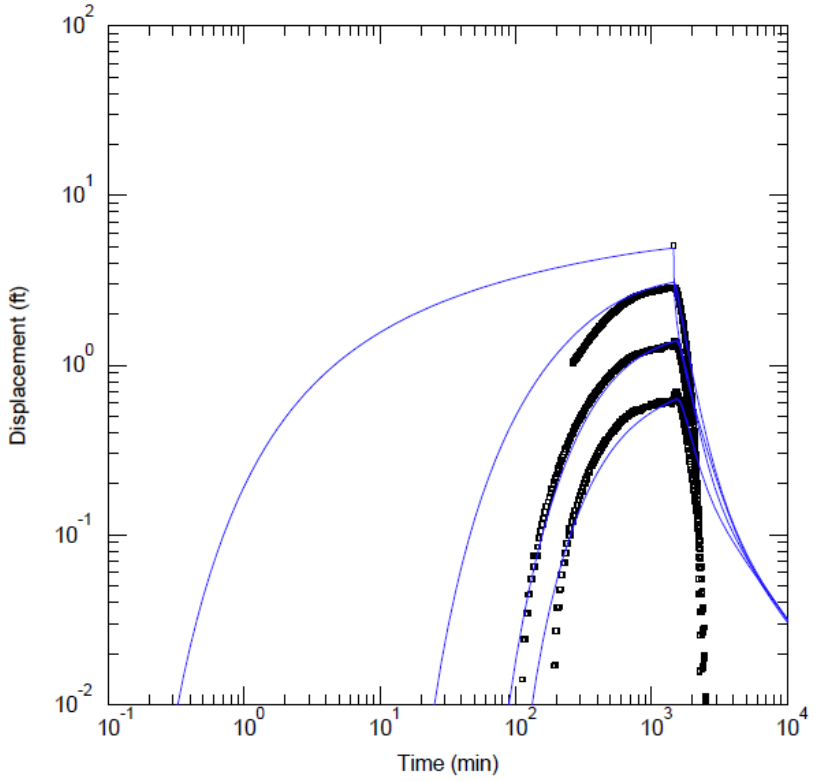
Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 2300. ft^2/day
1/B = 0.002 ft^{-1}
T2 = 2000. ft^2/day

S = 0.0005
ß/r = 0.0035 ft^{-1}
S2 = 0.25

L = 500 feet
kv = 130 * (0.002)^2 * 2300 = 1.2 ft/day

Figure 16. Solution of Aquifer Properties by Aqtesolv. Data from USGS 2-B, 2-C, and 2-E only



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-2_neuman_no2-D.aqt
Date: 08/22/17 Time: 14:45:40

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-E	51.7	0
USGS 2-C	53.2	0
USGS 2-B	54.8	0

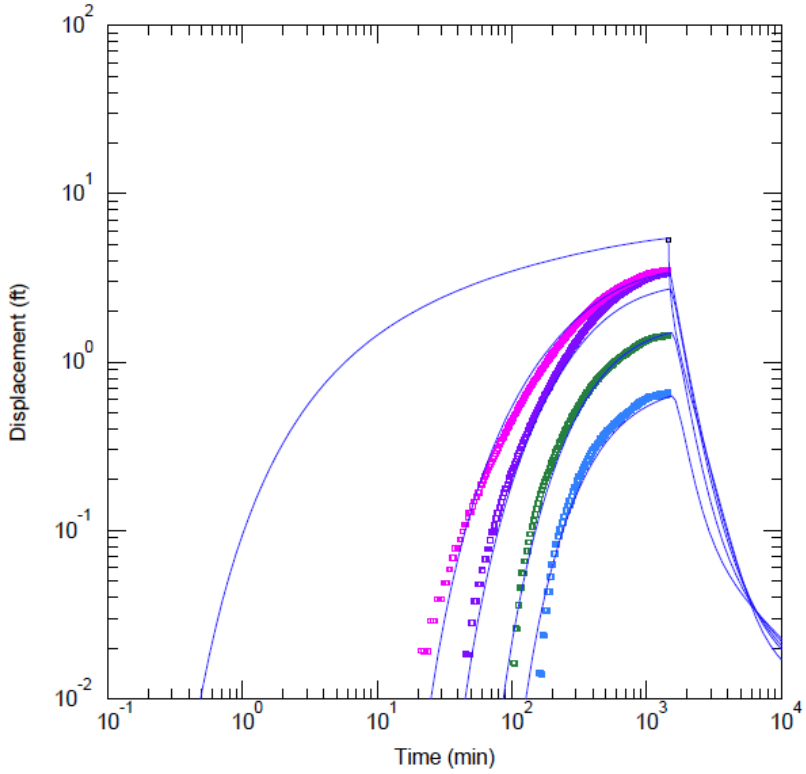
SOLUTION

Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 2700. ft^2/day
1/B = 0.0015 ft^{-1}
T2 = 10000. ft^2/day
S = 0.003
ß/r = 0.0007 ft^{-1}
S2 = 0.03

L = 670 feet
kv = 130 * (0.0015)^2 * 2700 = 0.79 ft/day

Figure 17. Solution of Aquifer Properties by Aqtesolv. Recovery Phase Data from USGS 2-B, 2-C, 2-D, and 2-E



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-2_neuman_no2-D_recovery.aqt
Date: 08/21/17 Time: 08:14:53

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-E	51.7	0
USGS 2-C	53.2	0
USGS 2-B	54.8	0
USGS 2-D	46	0

SOLUTION

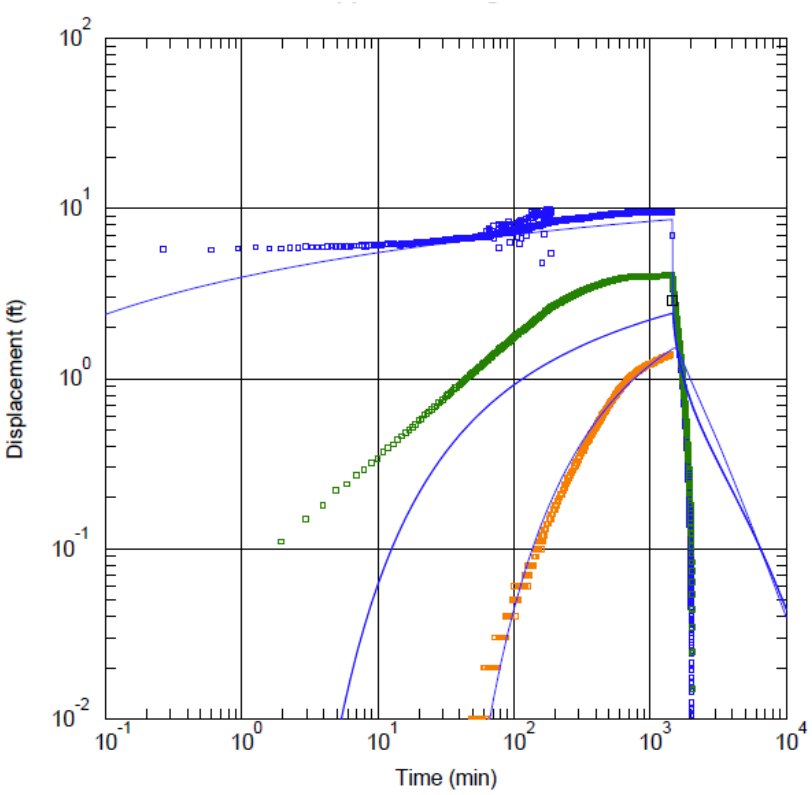
Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 2300. ft^2/day
1/B = 0.0017 ft^{-1}
T2 = 10000. ft^2/day

S = 0.004
ß/r = 0.0007 ft^{-1}
S2 = 0.2

L = 590 feet
kv = 130 * (0.0017)^2 * 2300 = 0.86 ft/day

Figure 18. Solution of Aquifer Properties by Aqtesolv. Match to Data from USGS 1-A, Data from USGS 1-B, and Cromwell 4



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-1_neuman.aqt
Date: 08/22/17 Time: 15:14:42

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0
1-B	140.5	0
1-A	142	0
Nest 1	141	0

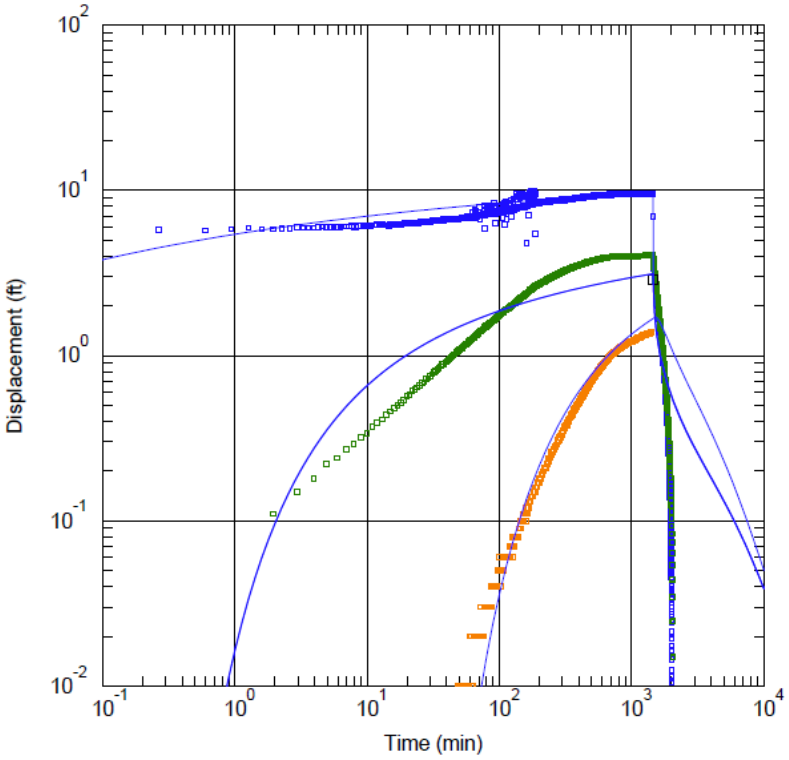
SOLUTION

Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 3731.6 ft^2/day
1/B = 0.0006568 ft^{-1}
T2 = 1.44E+8 ft^2/day
S = 0.008047
ß/r = 0.0001826 ft^{-1}
S2 = 1.

L = 1520 feet
kv = 130 * (0.00066)^2 * 3730 = 0.21 ft/day

Figure 19. Solution of Aquifer Properties by Aqtesolv. Match to Data from USGS 1-A and Modeled Drawdown at the Base of Till, Data from USGS 1-B, and Cromwell 4



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-1_neuman_obws_only.aqt
Date: 08/22/17 Time: 09:35:30

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0
1-B	140.5	0
1-A	142	0
Nest 1	141	0

SOLUTION

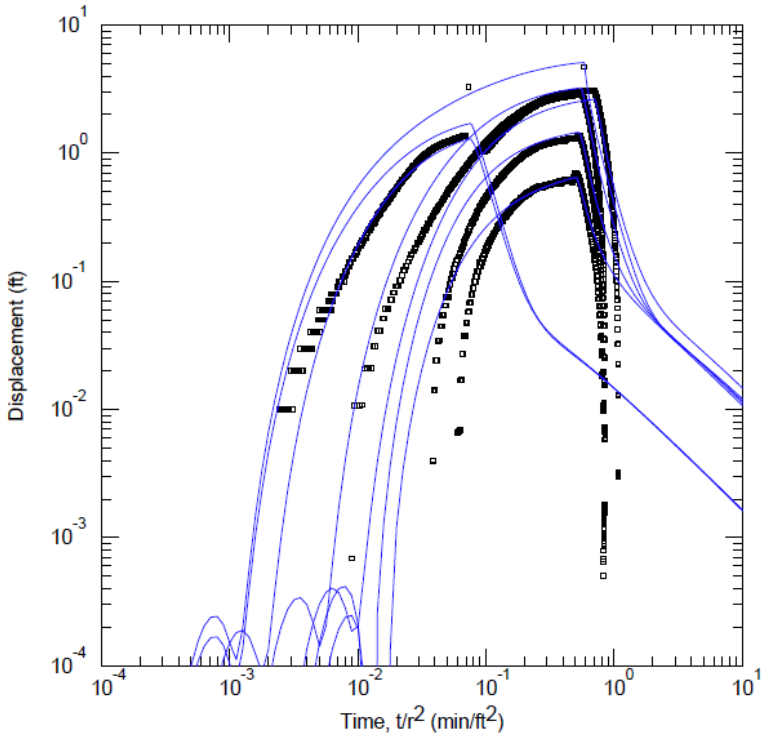
Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 3547.8 ft^2/day
1/B = 0.0005151 ft^{-1}
T2 = 2000. ft^2/day

S = 0.001231
ß/r = 0.0003916 ft^{-1}
S2 = 0.3

L = 1960 feet
kv = 130 * (0.00051)^2 * 3550 = 0.12 ft/day

Figure 20. Solution of Aquifer Properties by Aqtesolv. Match to Data from all USGS Observation Wells and Drawdown at the Base of Till at Nests 1 and 2



WELL TEST ANALYSIS

Data Set: O:\...\15_cromwell_nests1&2_neuman.aqt
Date: 08/22/17 Time: 15:22:35

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 0.5
Aquitard Thickness (b"): 1. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Nest 2	0	50
USGS 2-E	51.7	0
USGS 2-D	46	0
USGS 2-C	53.2	0
USGS 2-B	54.8	0
USGS 1-A	142	0
Nest 1	140.5	0

SOLUTION

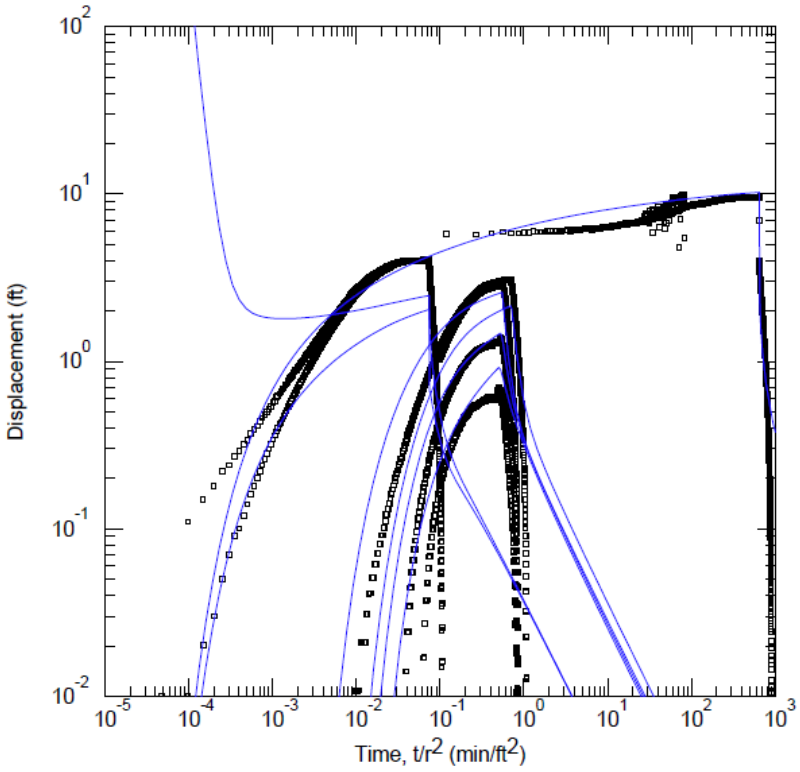
Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 1204.1 ft2/day
1/B = 0.006891 ft-1
T2 = 10000. ft2/day

S = 0.02603
ß/r = 0.001982 ft-1
S2 = 1.

L = 145 feet
kv = 130 * (0.00689)^2 * 1200 = 7.4 ft/day

Figure 21. Solution of Aquifer Properties by Aqtesolv. Match to all data



WELL TEST ANALYSIS

Data Set: O:\...\cromwell4_neuman_composite_thick.aqt
Date: 08/21/17 Time: 13:22:20

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 1.
Aquitard Thickness (b"): 20. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0
1-B	140.5	0
1-C	140.4	0
2-B	0	54.8
2-C	0	53.2
2-D	0	46
2-E	0	51.7

SOLUTION

Aquifer Model: Leaky
Solution Method: Neuman-Witherspoon

T = 2785.3 ft^2/day
1/B = 0.002969 ft^{-1}
T2 = 2200. ft^2/day
S = 0.00291
ß/r = 0.002176 ft^{-1}
S2 = 0.03

Figure 22. Similarity in Slope of 1-A and 2-E

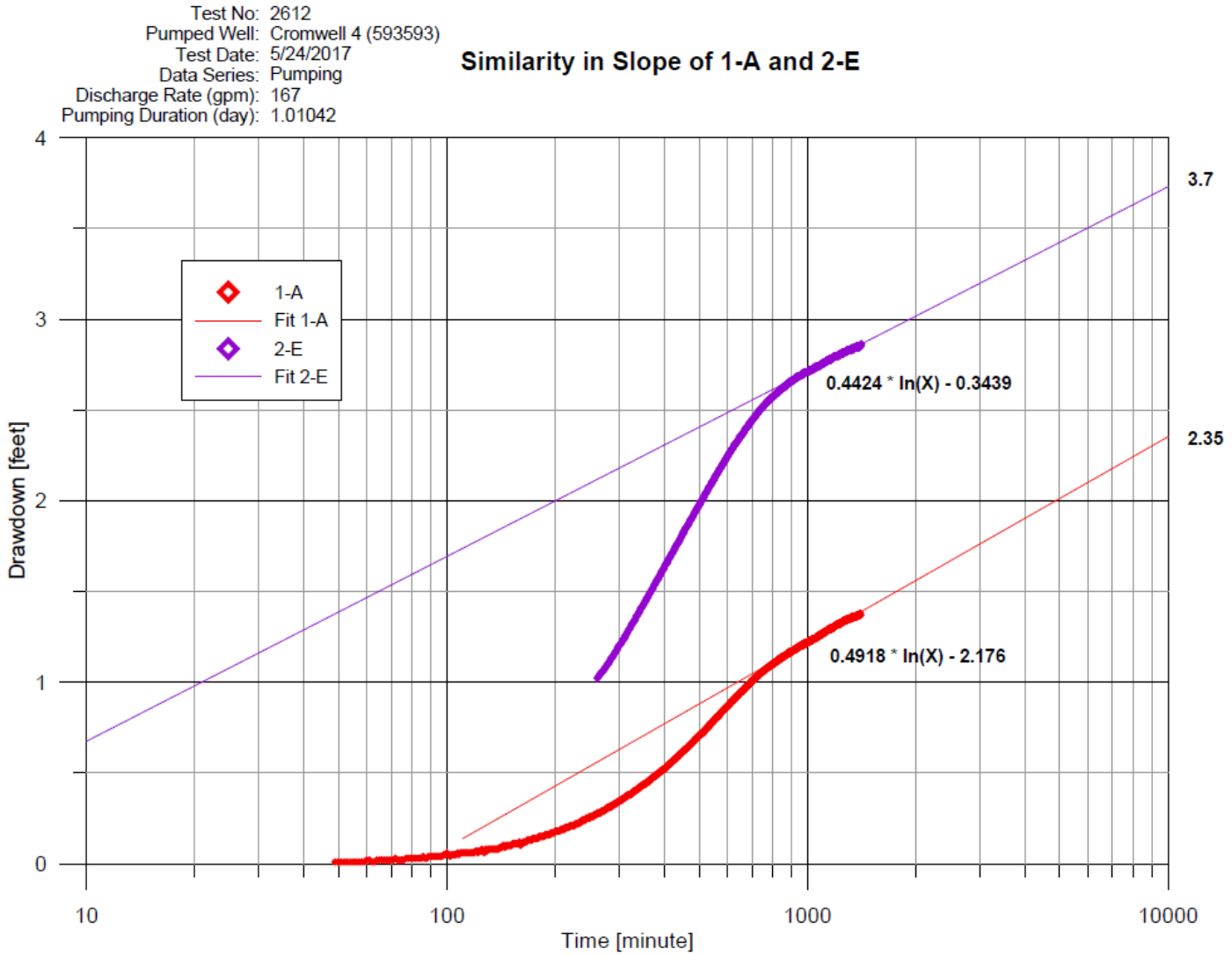
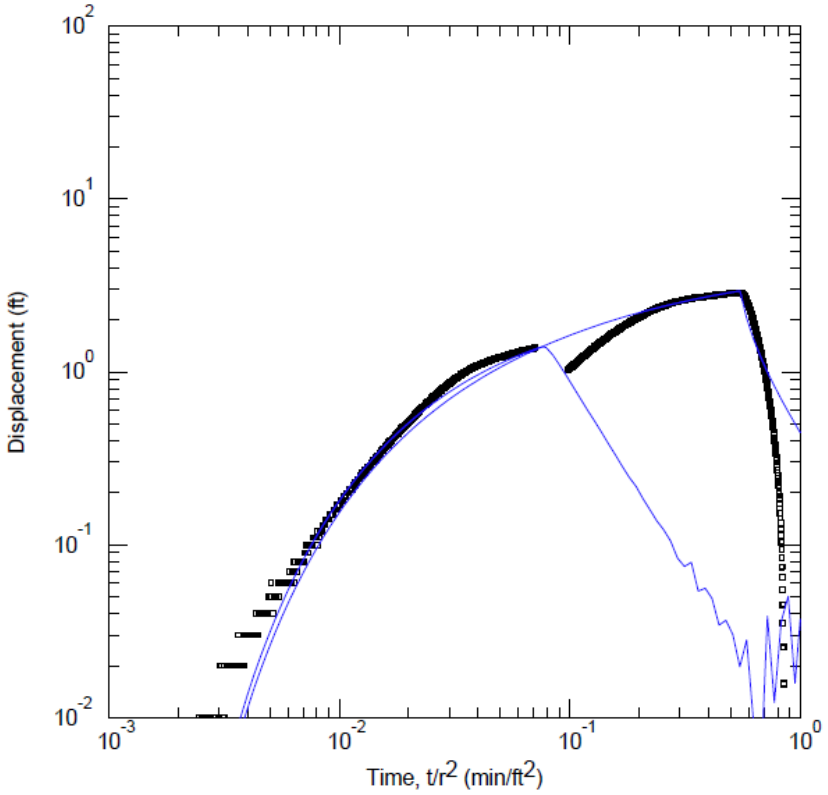


Figure 23. Solution of Aquifer Properties by Aqtesolv. Match to Data from USGS 1-A and USGS 2-E



WELL TEST ANALYSIS

Data Set: O:\...\24_cromwell4_1-A&2-E_neuman_composite.aqt
Date: 09/12/17 Time: 14:03:19

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 1.
Aquitard Thickness (b"): 20. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
1-A	140.6	0
2-E	0	51.7

SOLUTION

Aquifer Model: Leaky
T = 1589. ft^2/day
1/B = 0.004471 ft^{-1}
T2 = 10000. ft^2/day

Solution Method: Neuman-Witherspoon
S = 0.05497
ß/r = 7.276E-8 ft^{-1}
S2 = 0.3

L = 224 feet
kv = 130 * (0.00447)^2 * 1590 = 4.1 ft/day

Figure 24. Agarwal Analysis

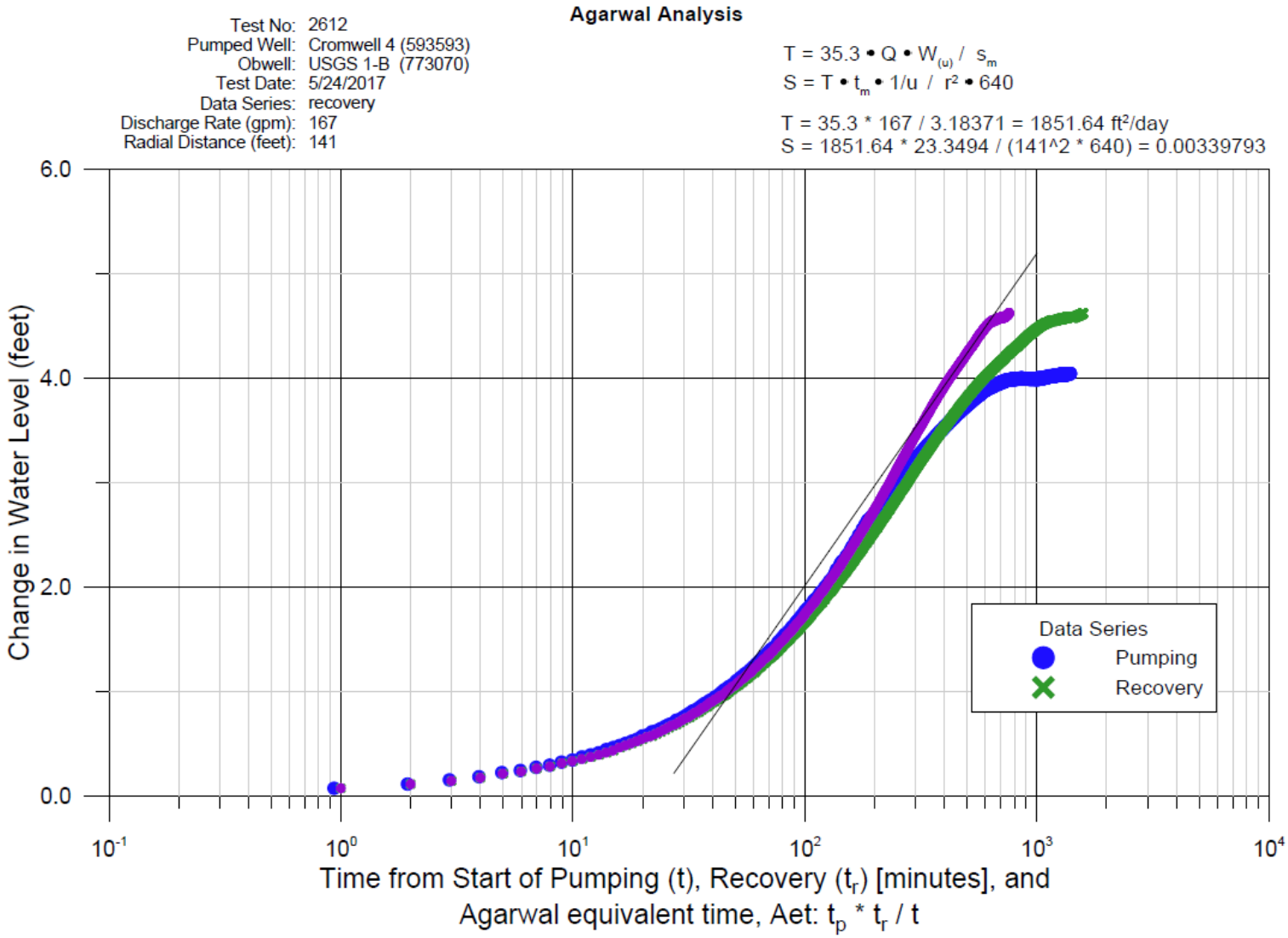
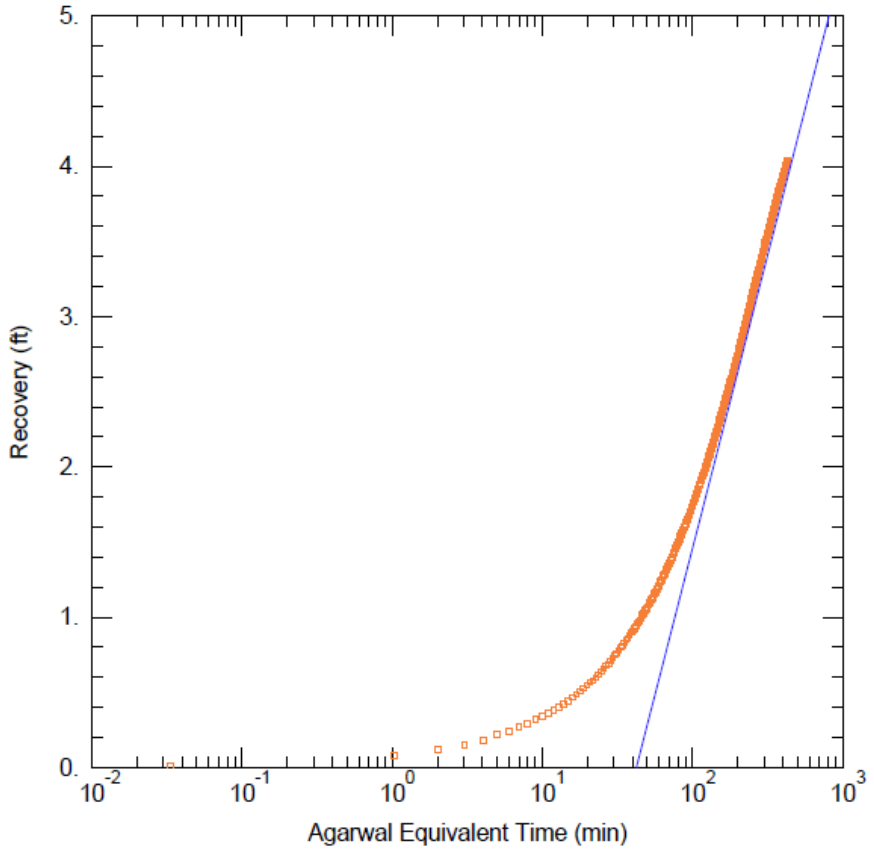


Figure 25. Solution of Aquifer Properties by Aqtesolv. Analysis of Recovery Data from Pumped Well



WELL TEST ANALYSIS

Data Set: O:\...\cromwell-4_nest-1-B_agarwal_theis.aqt
Date: 09/06/17 Time: 16:43:05

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft Anisotropy Ratio (Kz/Kr): 1.

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
1-B	140.5	0

SOLUTION

Aquifer Model: Confined Solution Method: Cooper-Jacob
T = 1511.4 ft^2/day S = 0.00504

Figure 26. Well Identification

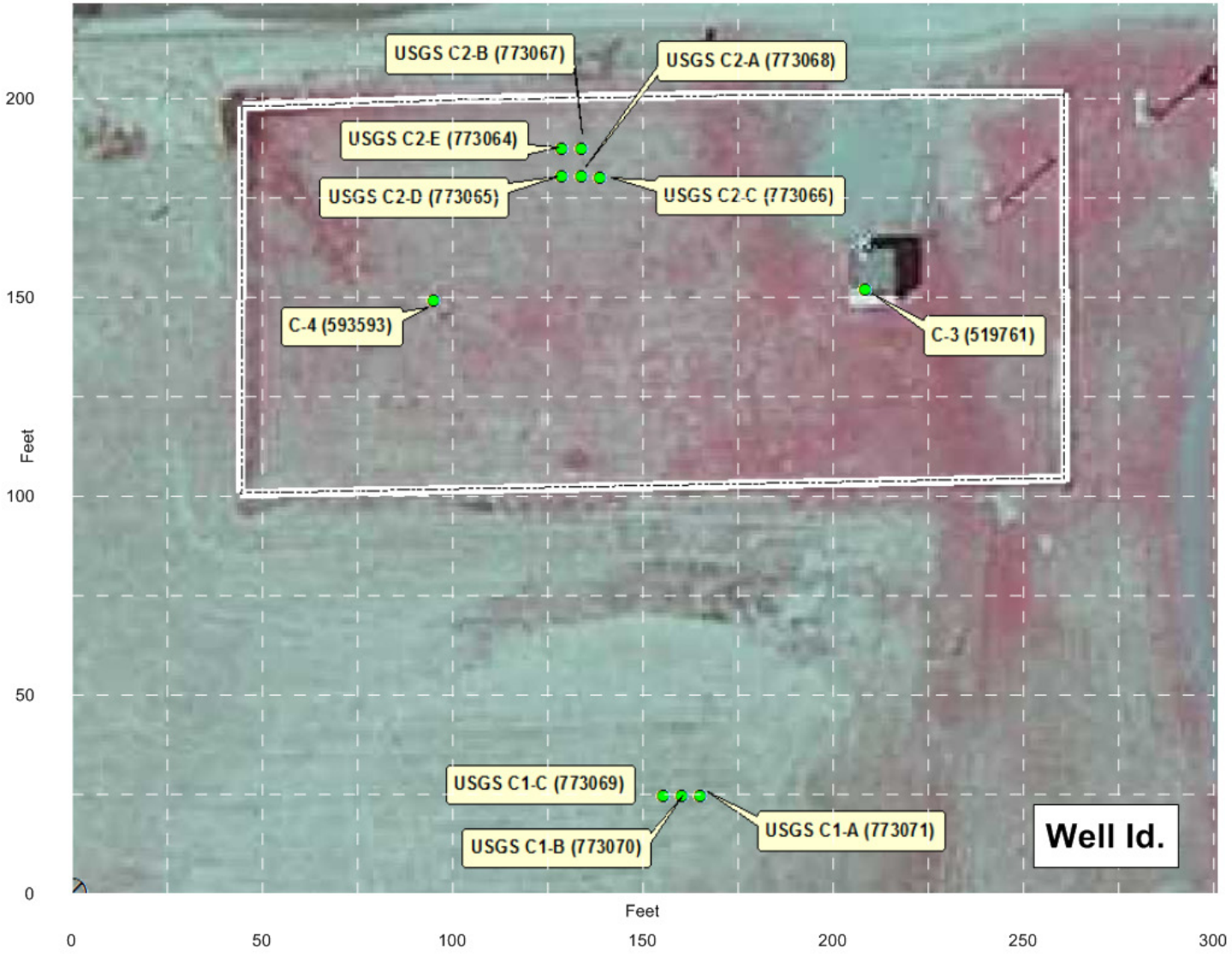


Figure 27. Distances between Wells and Well Nests

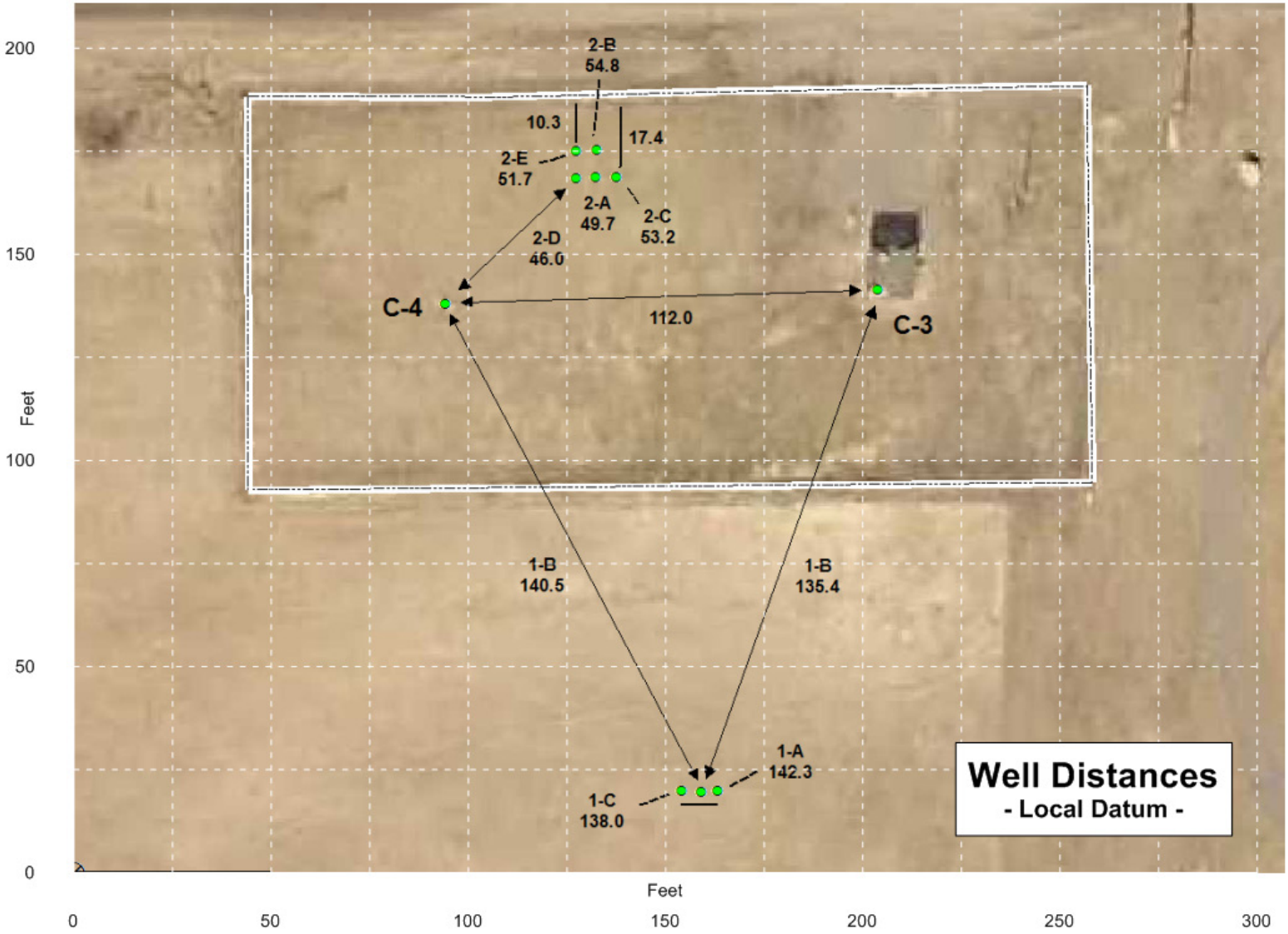
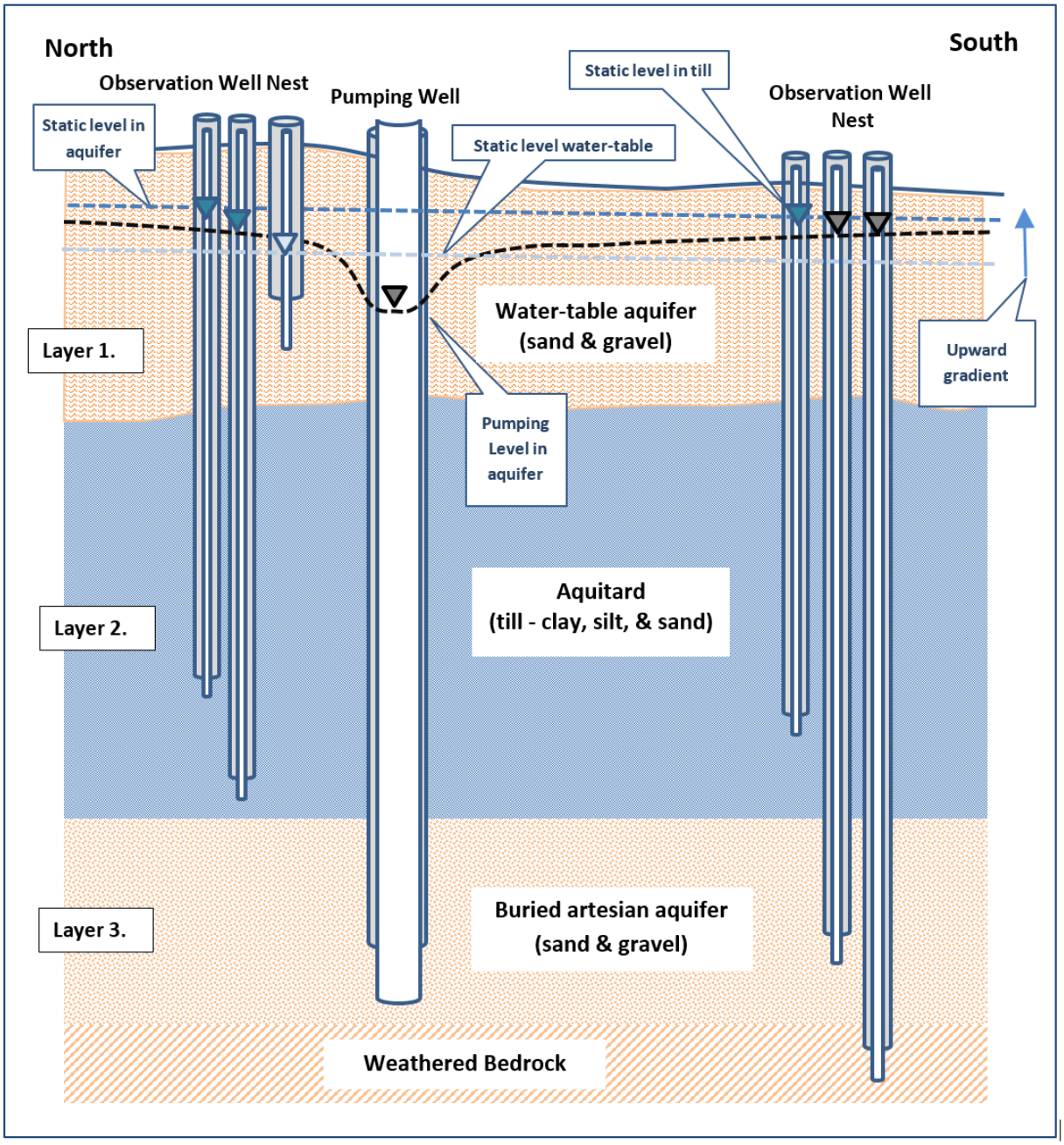


Figure 28. Schematic Section Across Site



Schematic Section

Figure 29. Time-series of Groundwater Elevation Collected at Cromwell 4.

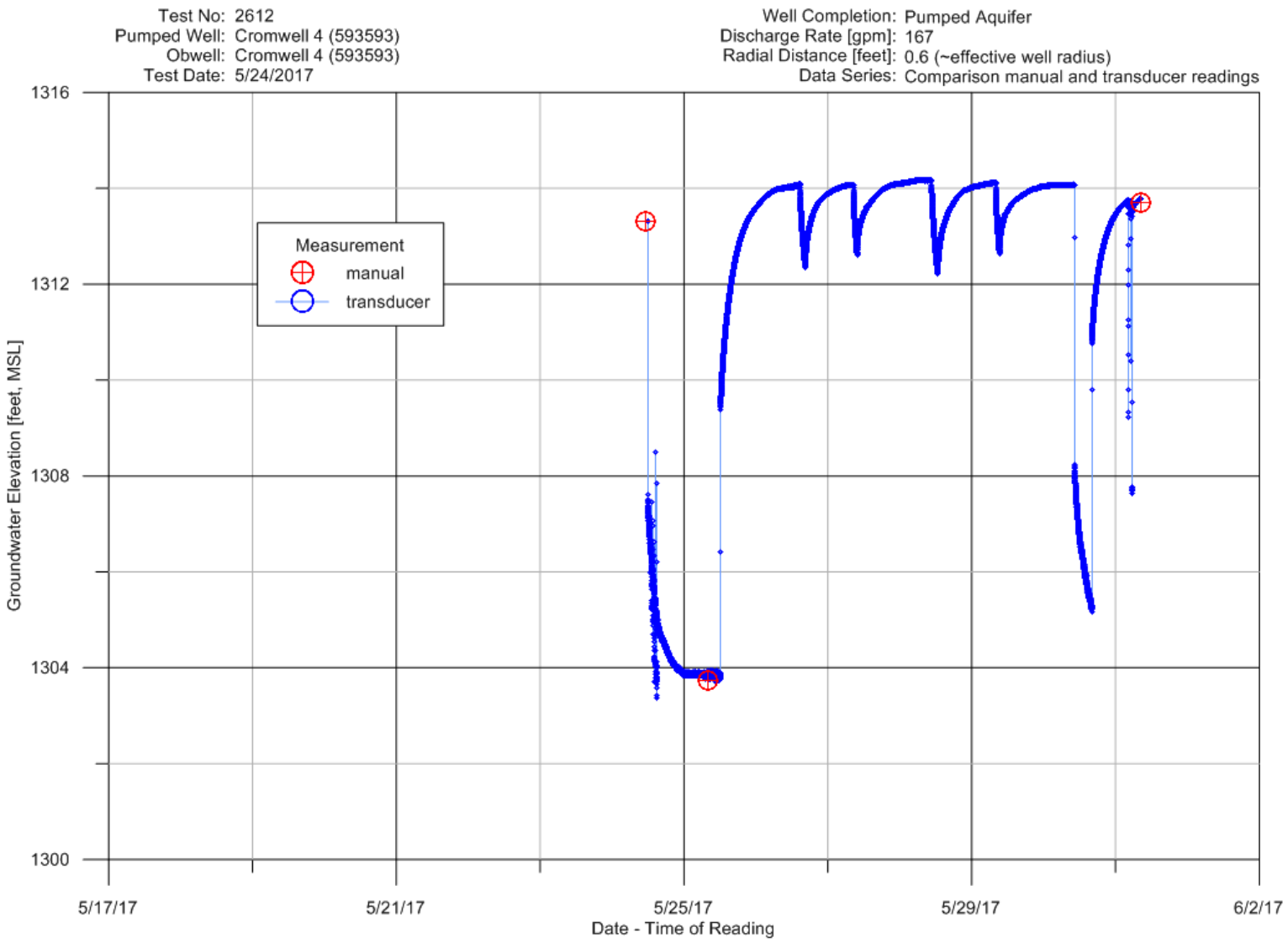


Figure 30. Time-series of Groundwater Elevation Collected at USGS 1-A.

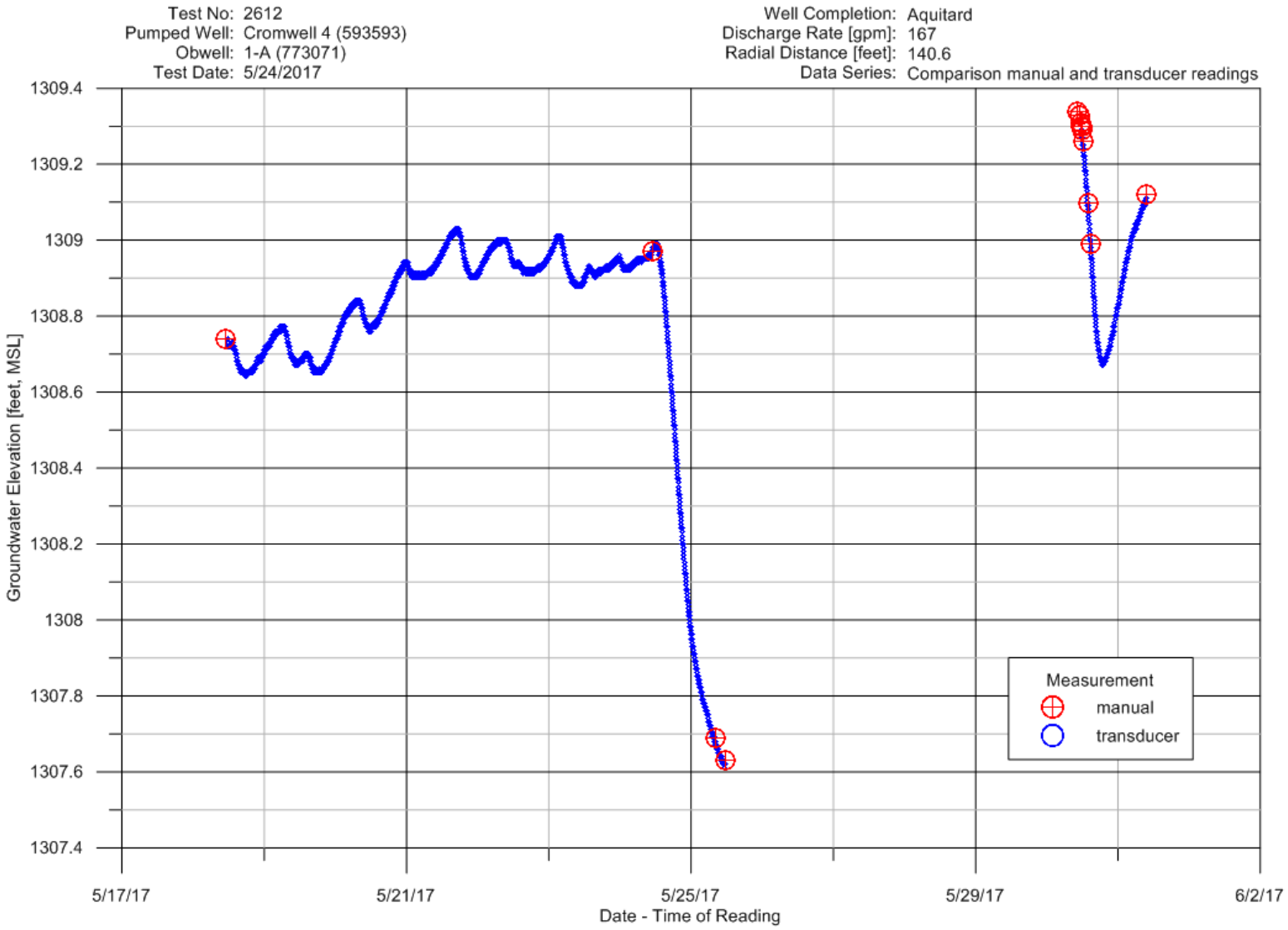


Figure 31. Time-series of Groundwater Elevation Collected at USGS 1-B

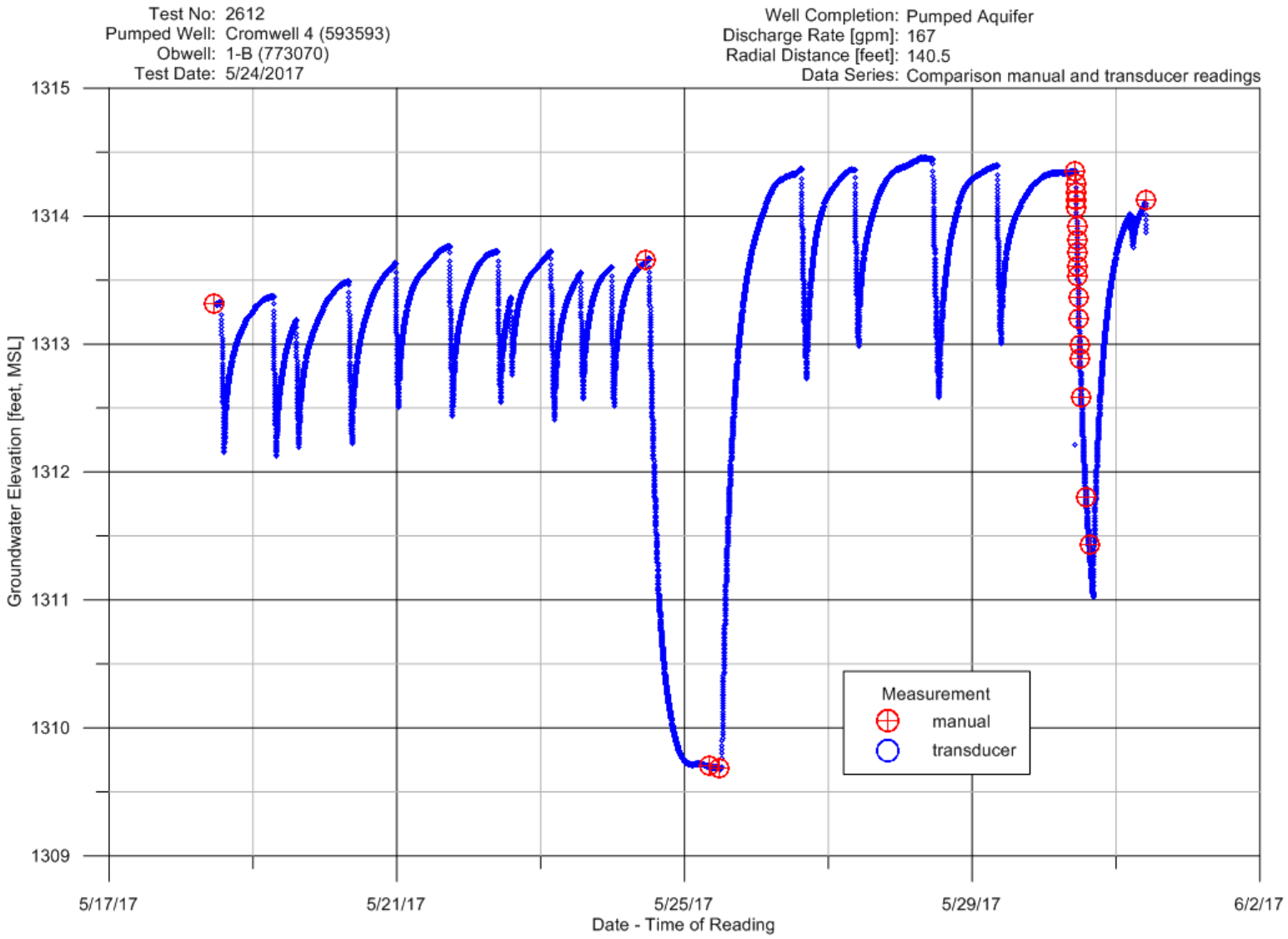


Figure 32. Time-series of Groundwater Elevation Collected at USGS 1-C

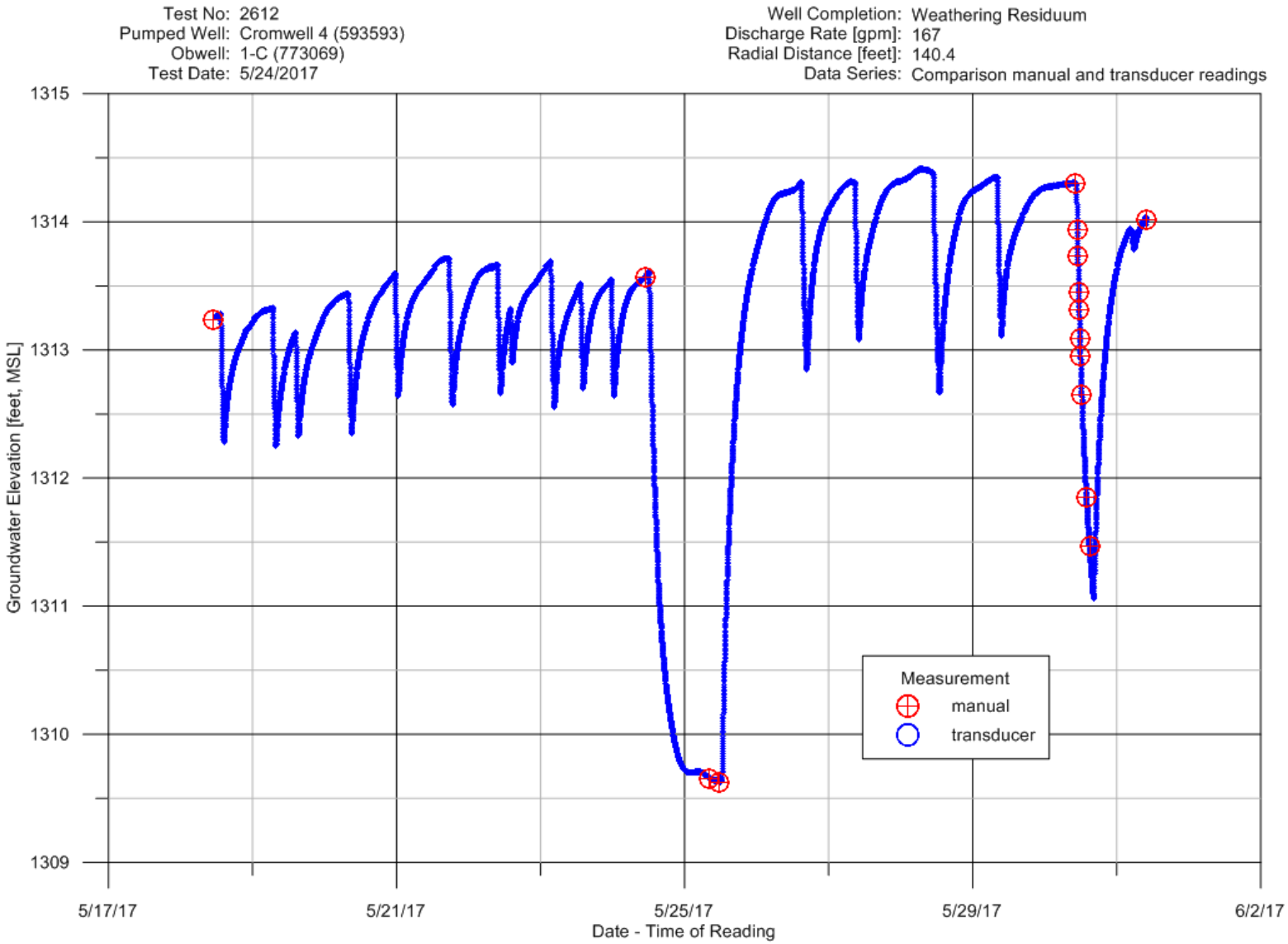


Figure 33. Time-series of Groundwater Elevation Collected at USGS 2-A

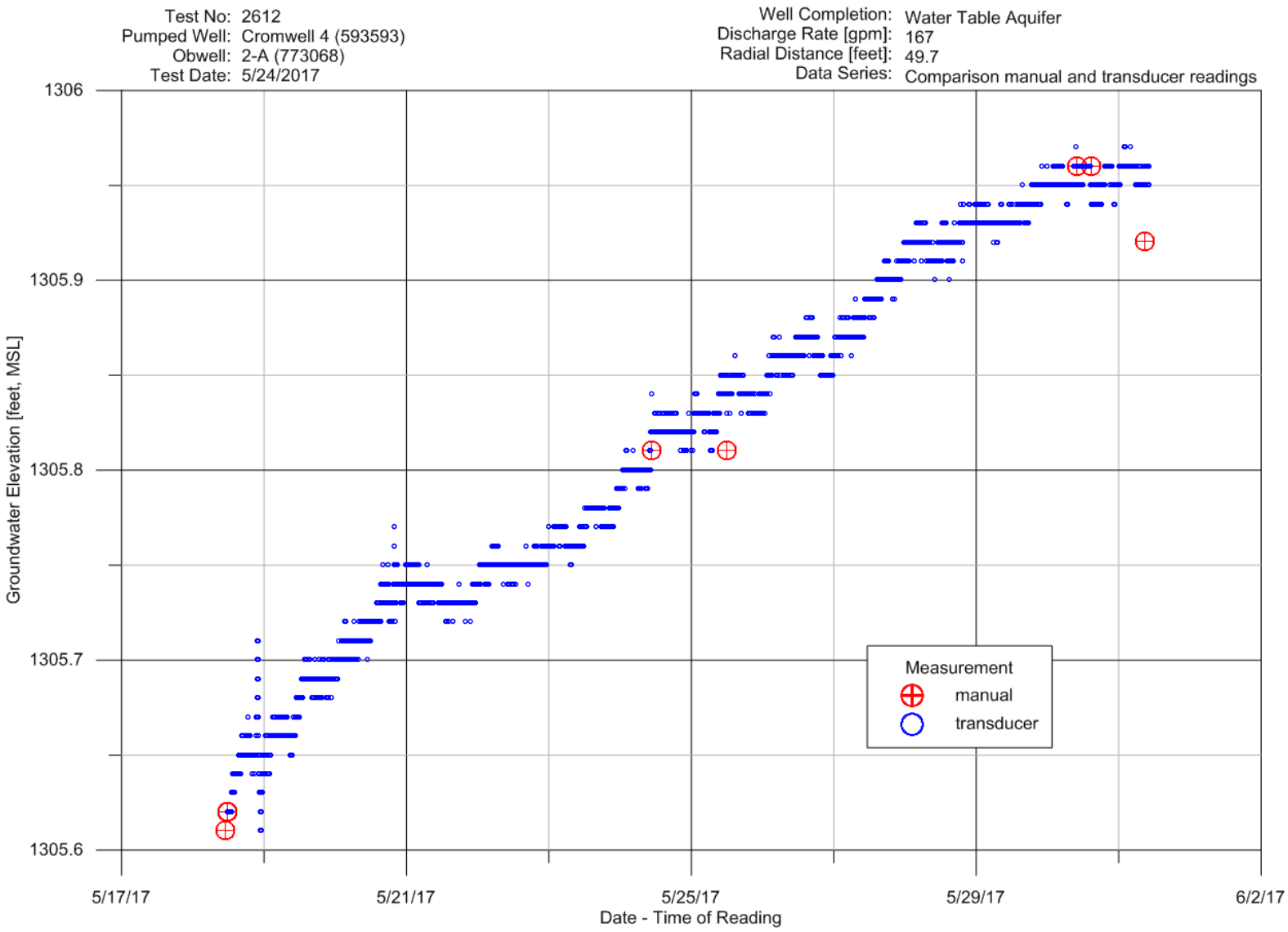


Figure 34. Time-series of Groundwater Elevation Collected at USGS 2-B

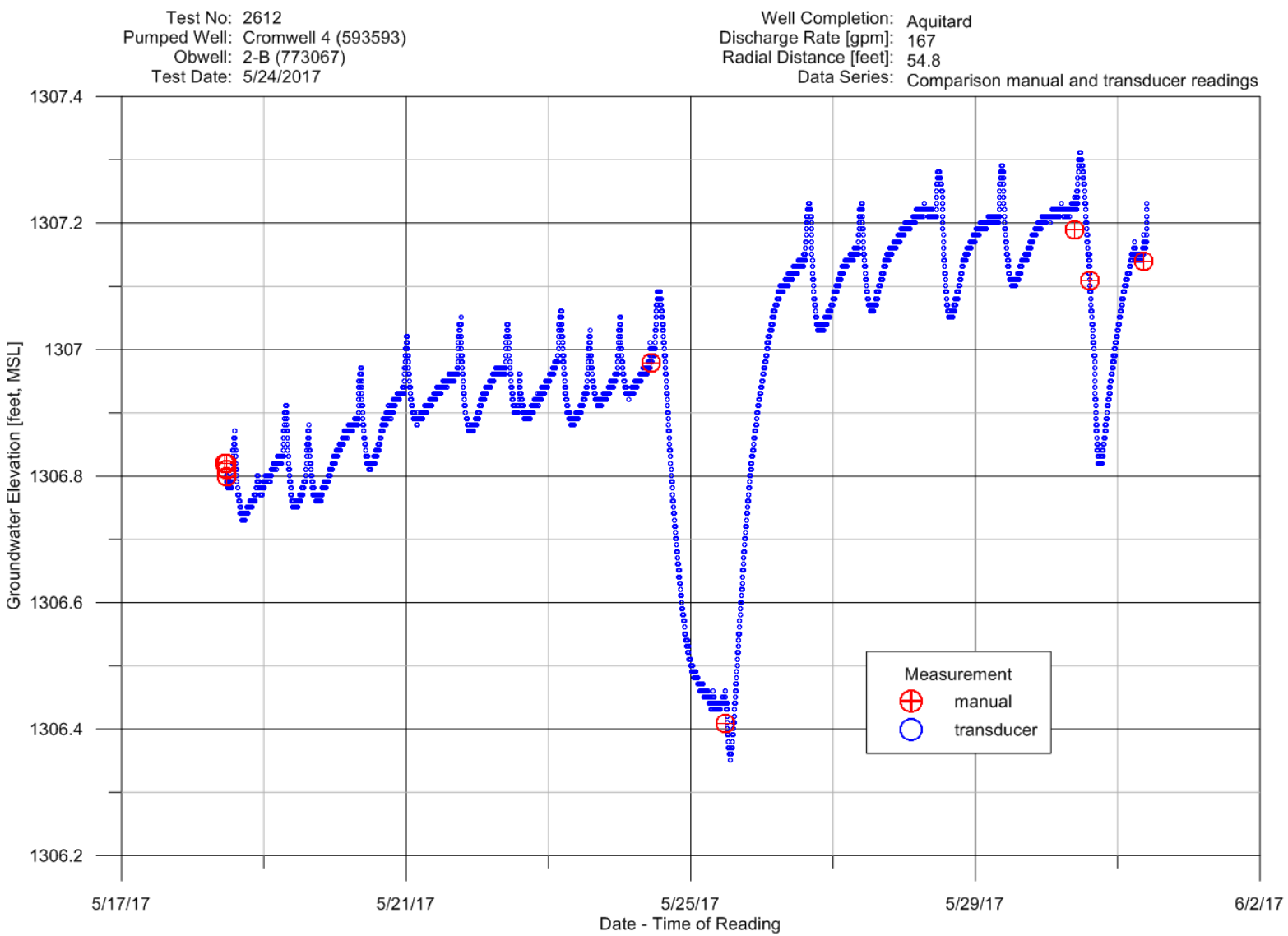


Figure 35. Time-series of Groundwater Elevation Collected at USGS 2-C

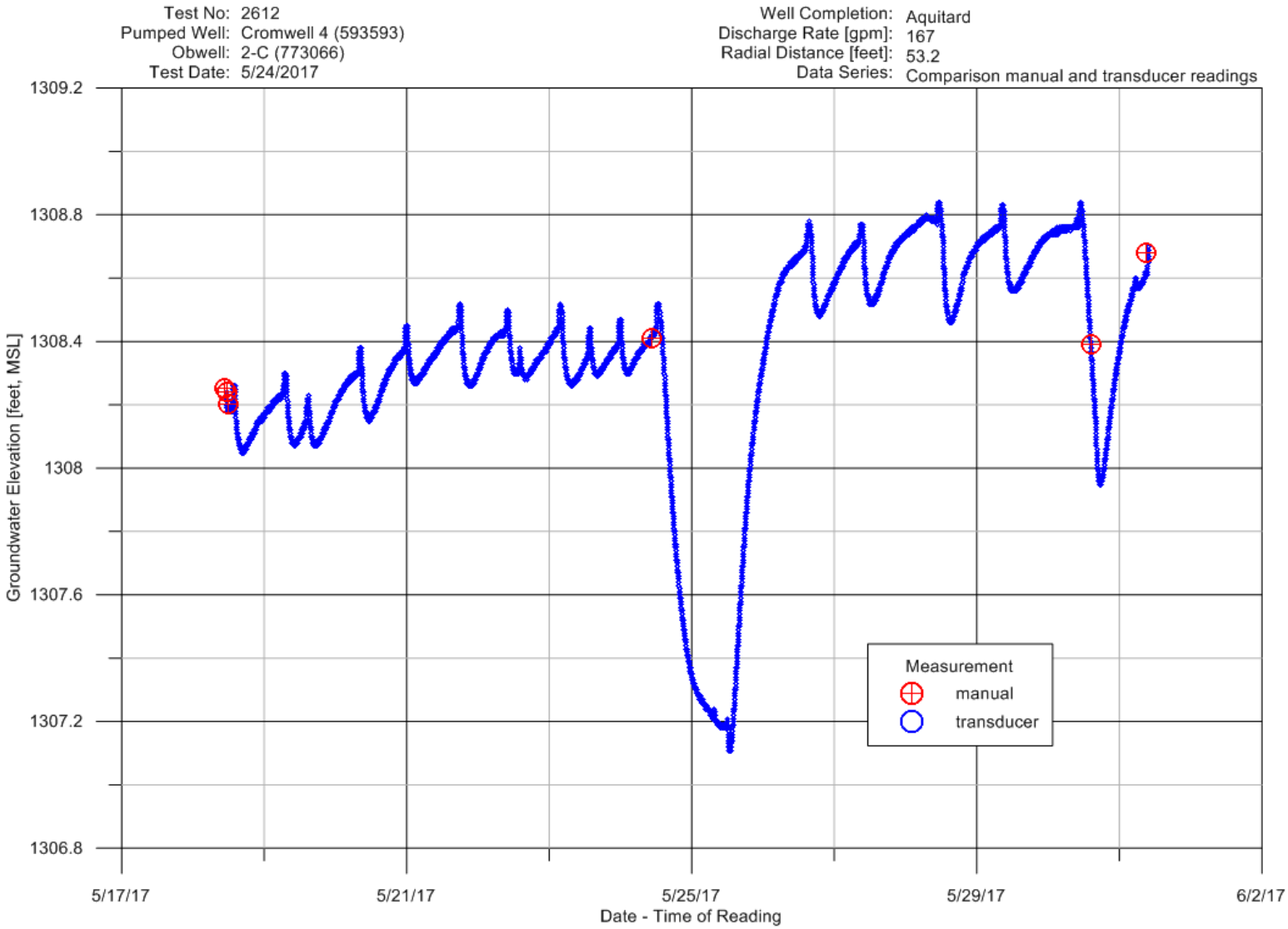


Figure 36. Time-series of Groundwater Elevation Collected at USGS 2-D

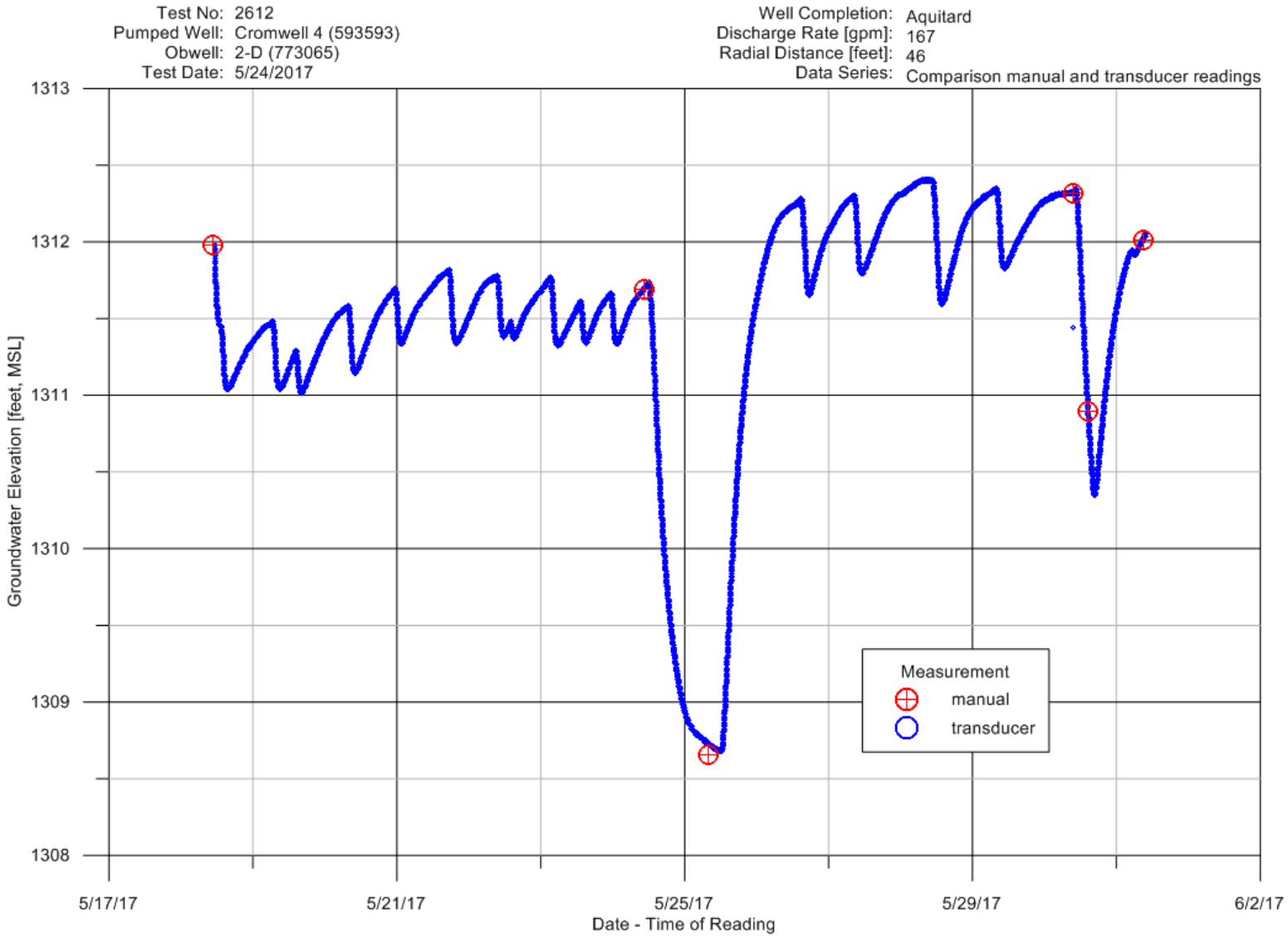


Figure 37. Time-series of Groundwater Elevation Collected at USGS 2-E

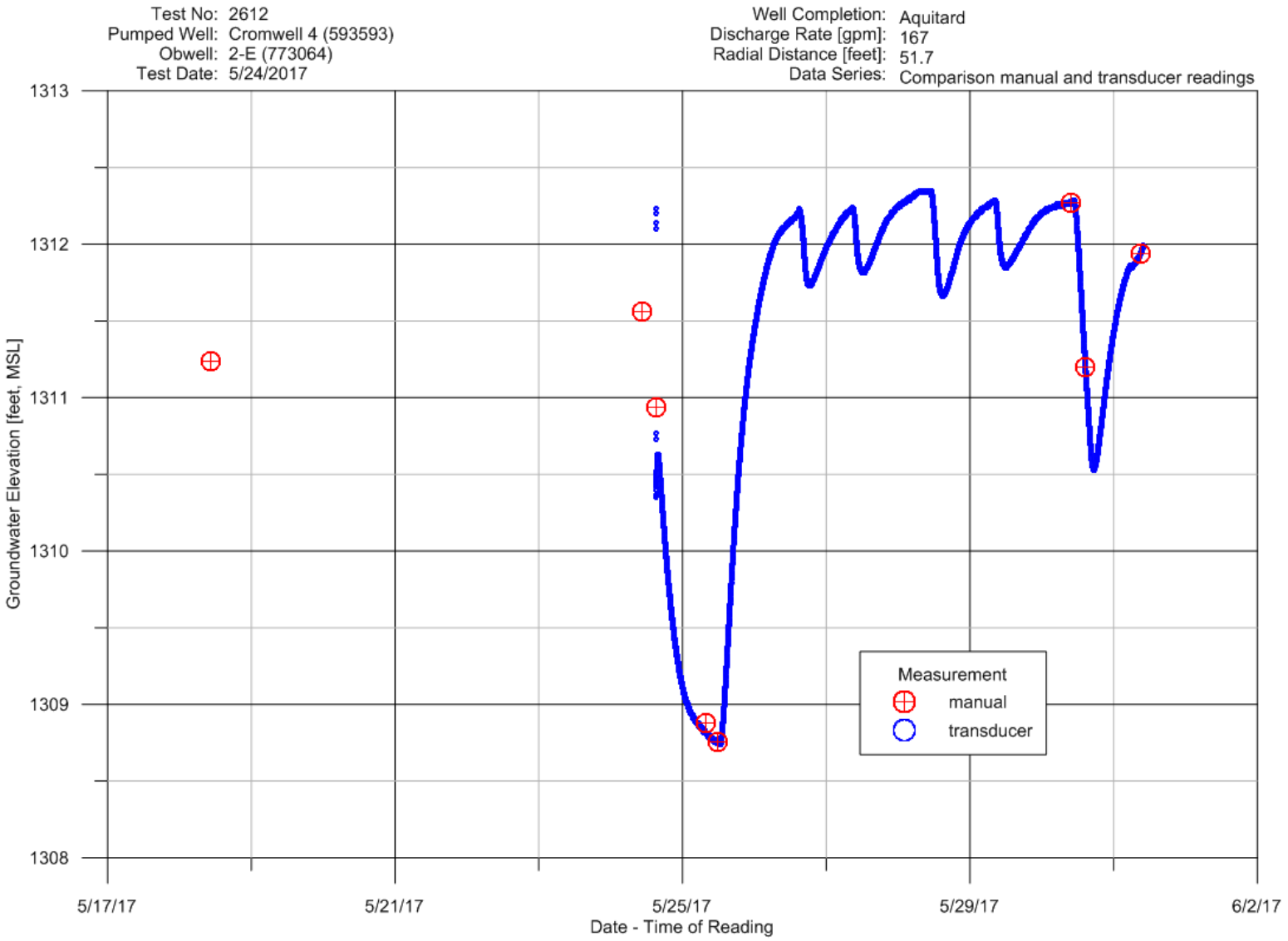


Figure 38. Time-series of Groundwater Elevation Collected at all Wells

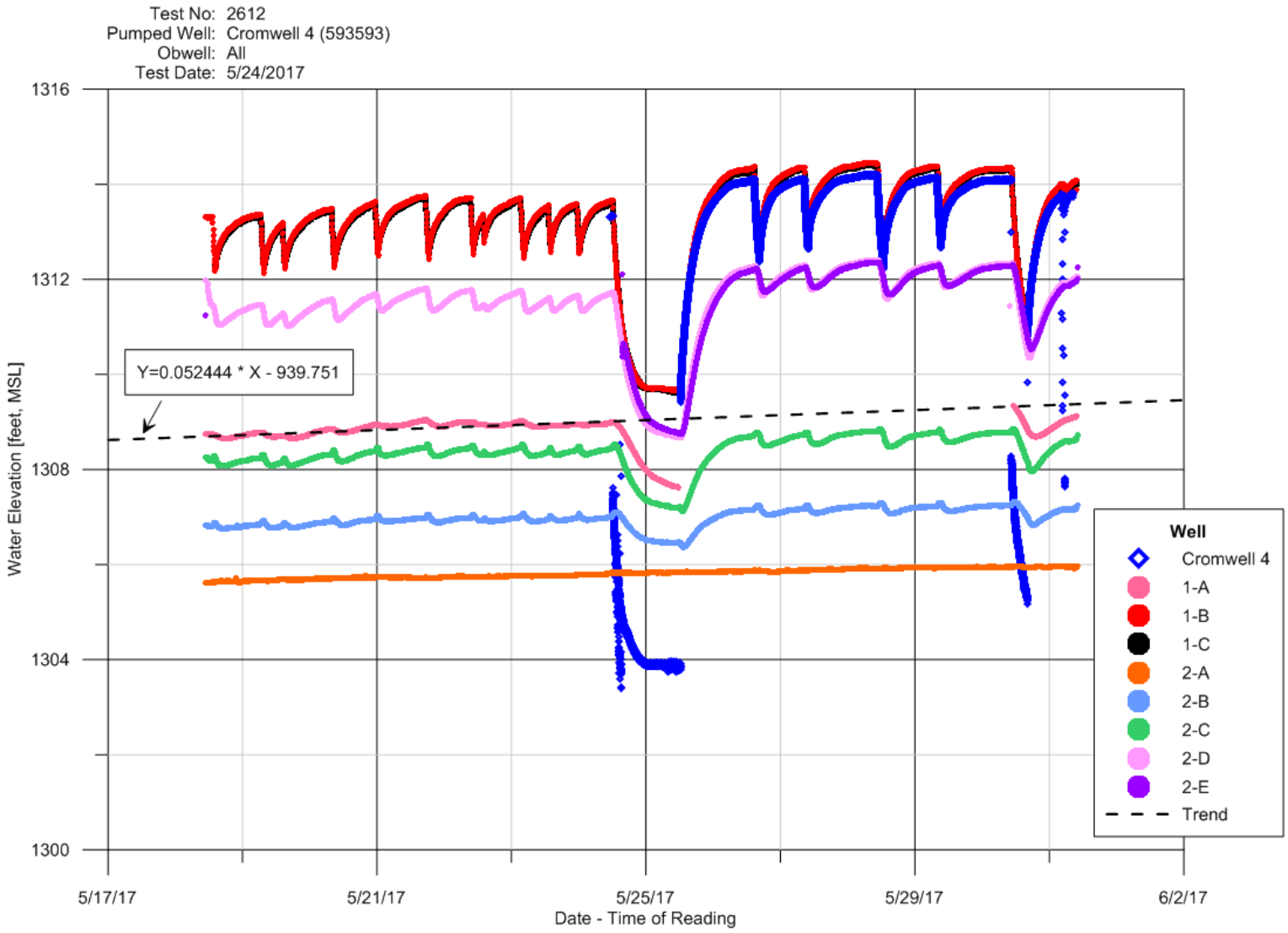


Figure 39. Time-series of Groundwater Elevation Collected at Cromwell 4 and Nest 1

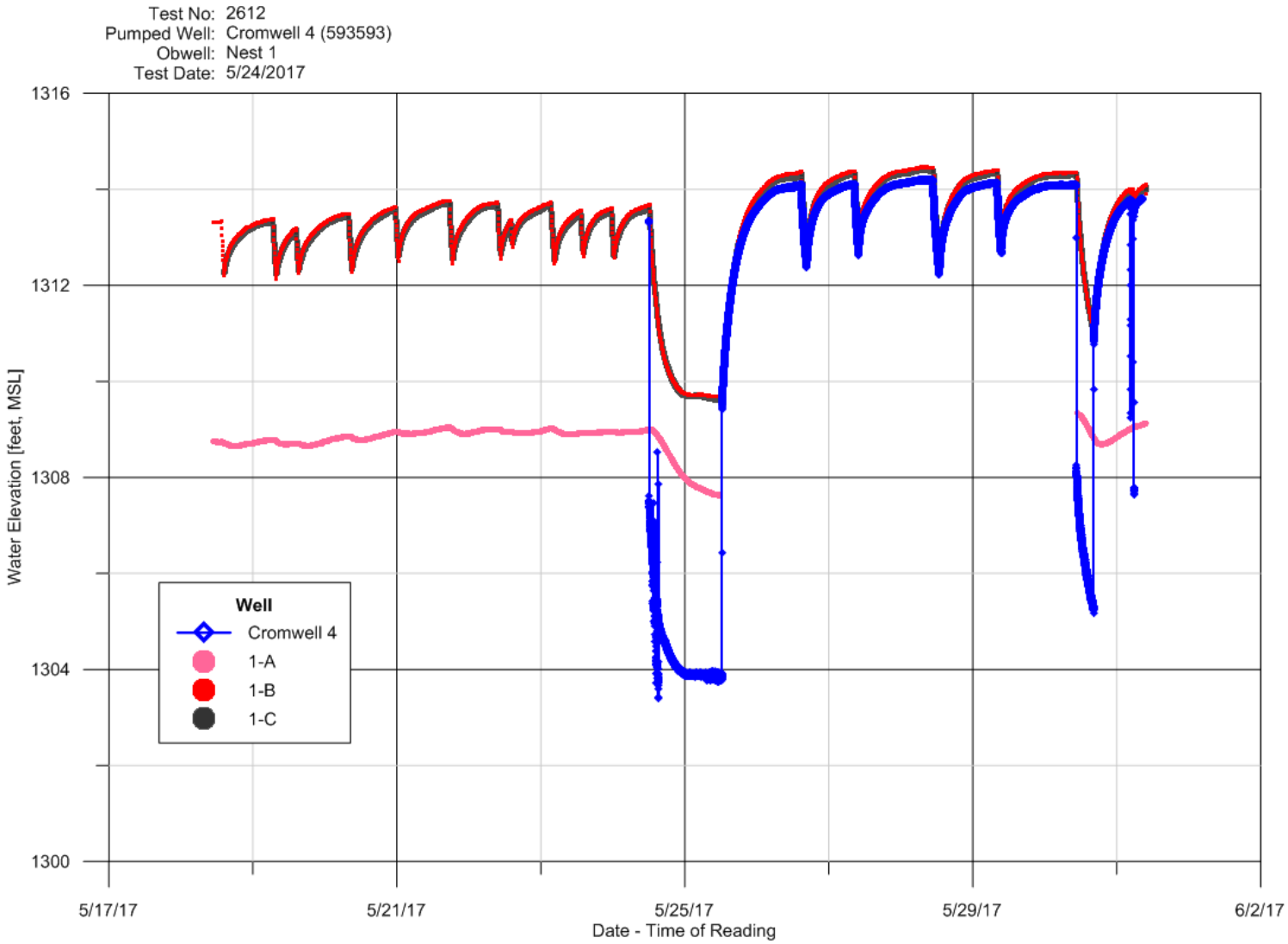


Figure 40. Time-series of Groundwater Elevation Collected at Cromwell 4 and Nest 2

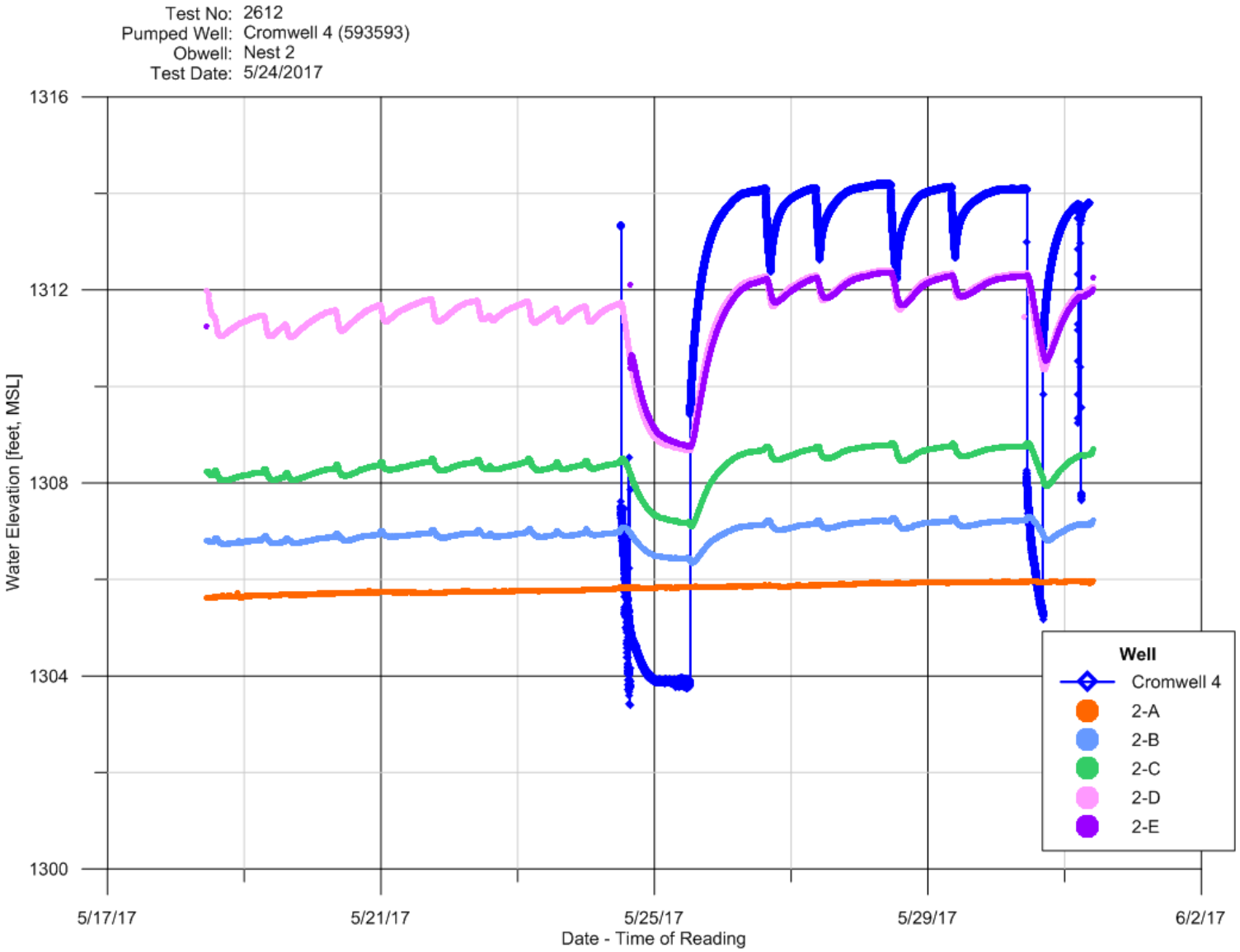


Figure 41. Time-series of Groundwater Elevation Collected at USGS 2-A and Barometric Pressure as Difference in Water Level

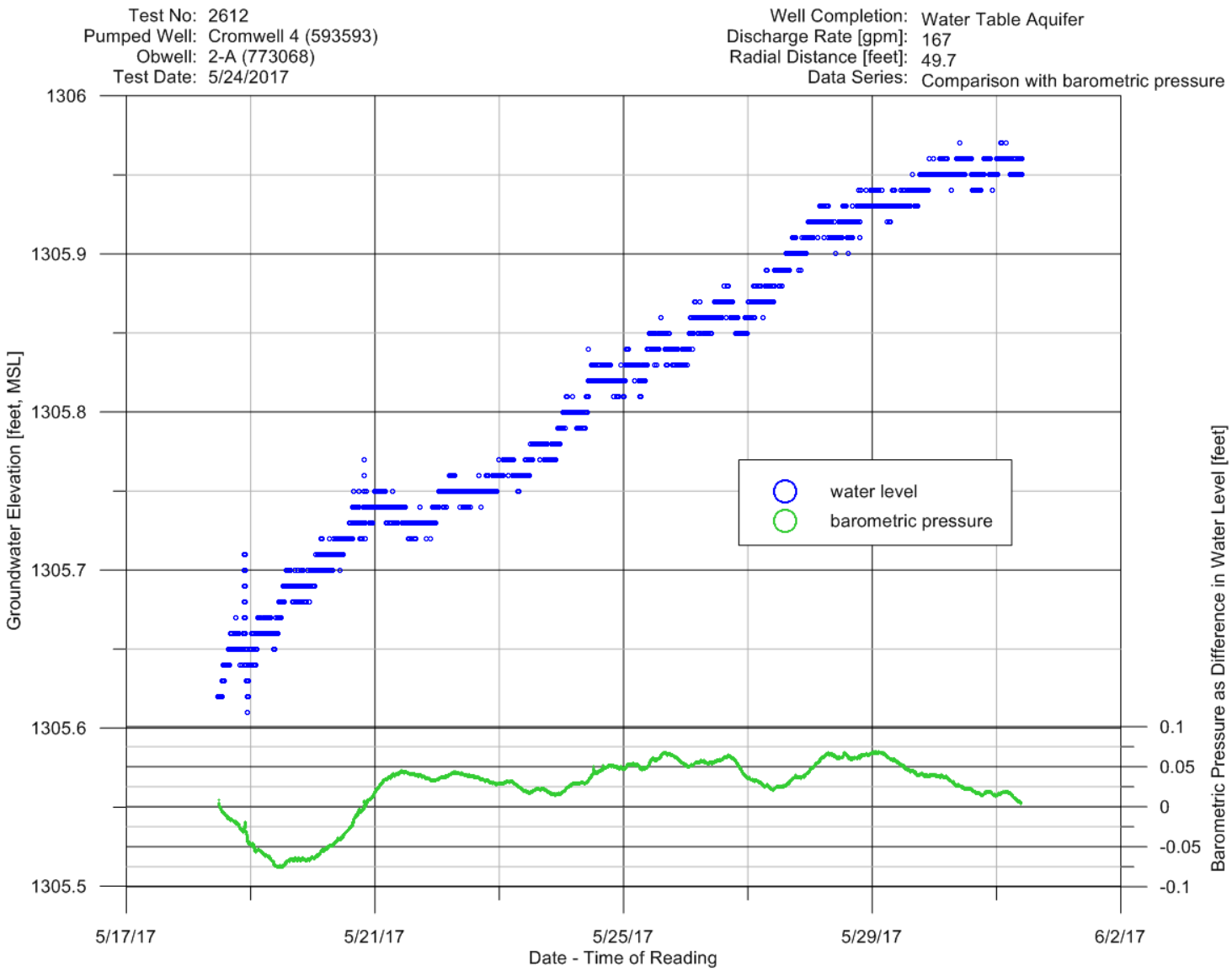
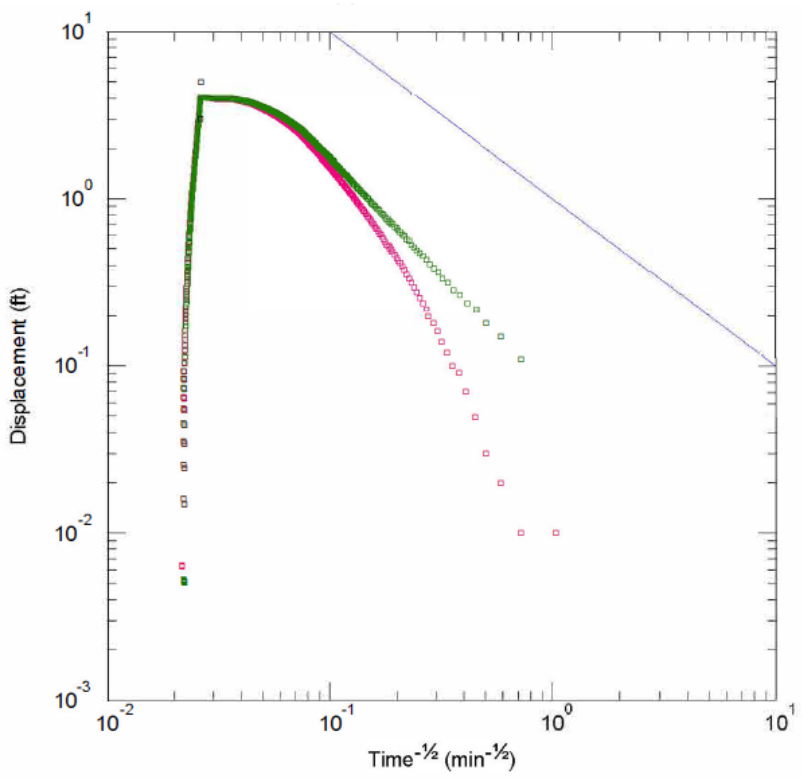


Figure 42. Aqtesolv plot of diagnostic slope for spherical flow and data from USGS 1-B and 1-C



WELL TEST ANALYSIS

Data Set: O:\...\cromwell_nest-1_hantush_partial_1-Bonly_spherical.aqt
Date: 08/18/17 Time: 16:44:40

PROJECT INFORMATION

Company: MDH
Client: City of Cromwell
Location: Cromwell 4
Test Well: C-4 (593593)
Test Date: 5/24/2017

AQUIFER DATA

Saturated Thickness: 145. ft
Aquitard Thickness (b'): 130. ft
Anisotropy Ratio (Kz/Kr): 1.
Aquitard Thickness (b"): 20. ft

WELL DATA

Pumping Wells

Well Name	X (ft)	Y (ft)
Cromwell 4	0	0

Observation Wells

Well Name	X (ft)	Y (ft)
1-C	139	0
1-B	140.5	0
1-A	142	0
Nest 1	141	0
Nest 2	0	50

SOLUTION

Aquifer Model: Leaky
T = 1043.9 ft^2/day
1/B = 0.004064 ft^{-1}
C = 0. min^2/ft^5

Solution Method: Hantush-Jacob
S = 0.005146
Sw = 0.
P = 2.

Step Test Model: Jacob-Rorabaugh
Time (t) = 1. min Rate (Q) in cu. ft/min

s(t) = 5.641E-19Q + 0.Q$^{2.}$
W.E. = 100.% (Q from last step)

Figure 43. Conventional log-log plot of drawdown and recovery at USGS 1-B with Walton (1960) leaky type-curve

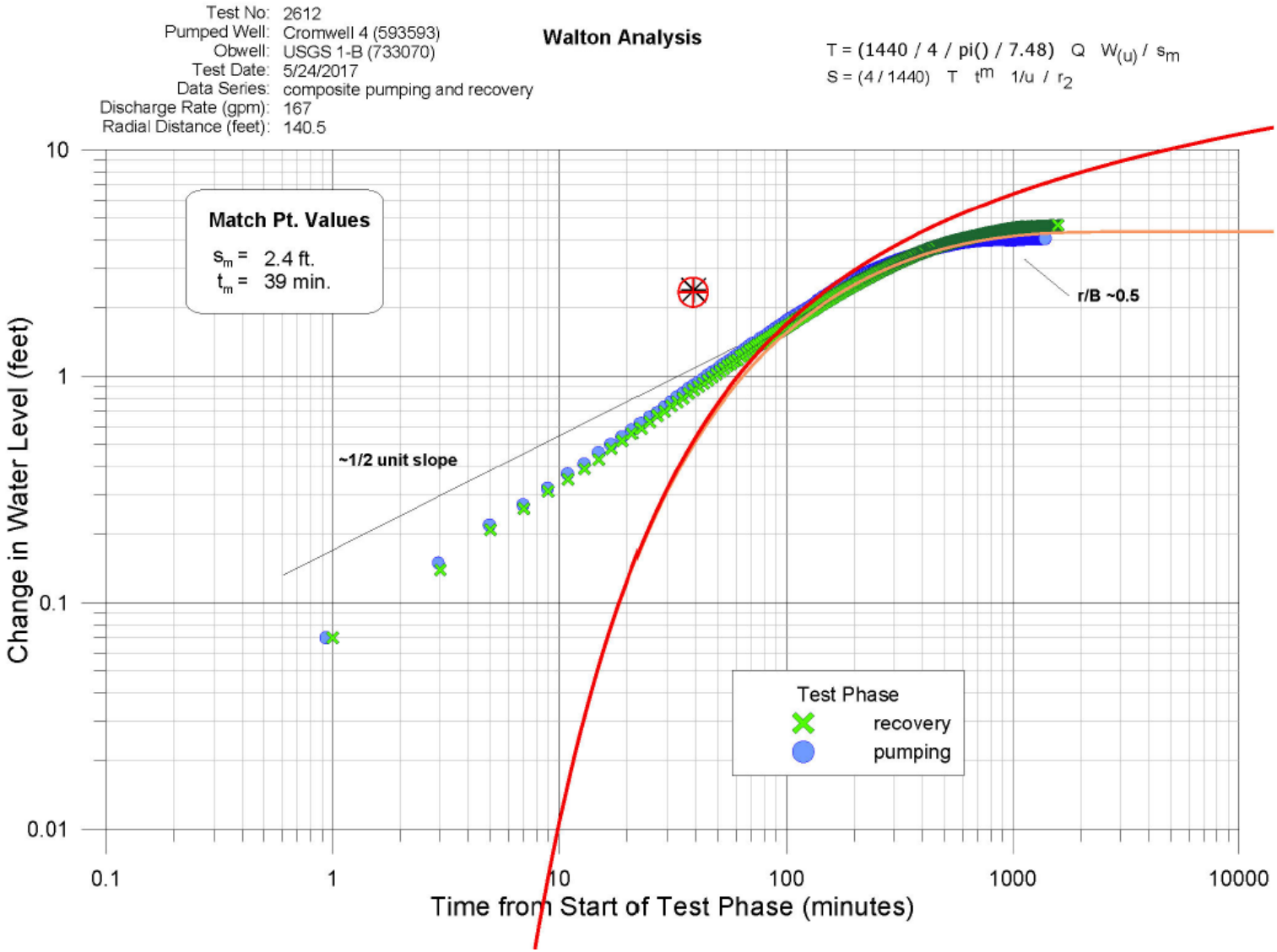


Figure 44. Conventional log-log plot of drawdown and recovery at USGS 1-C with Walton (1960) leaky type-curve

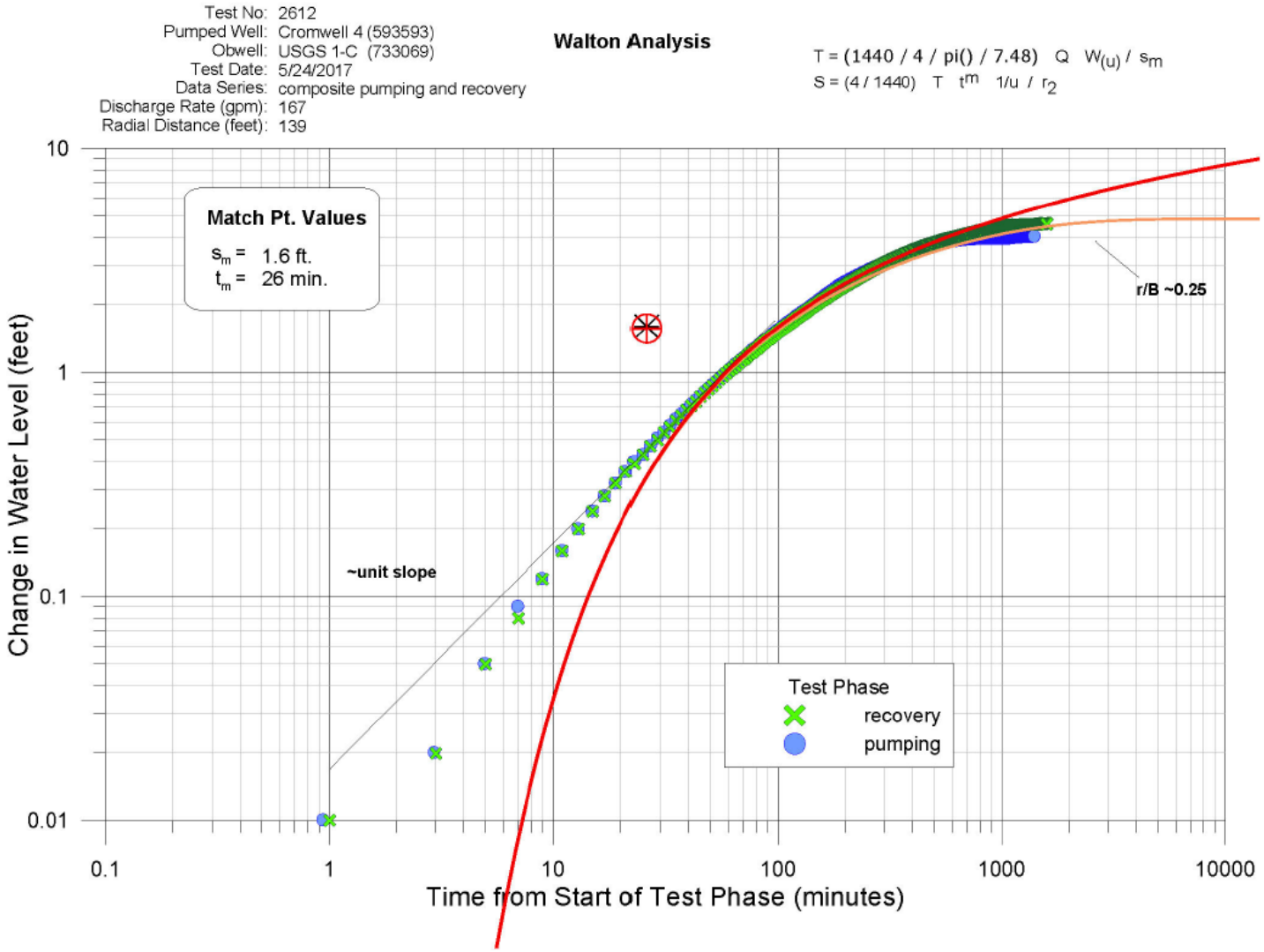


Figure 45. Well and Boring Report - Well 593593

Minnesota Unique Well Number: **593593**

County: Carlton
Quad: Cromwell
Quad ID: 226B

MINNESOTA DEPARTMENT OF HEALTH

WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

Entry Date: 03/22/2000
Update Date: 03/10/2014
Received Date:

Well Name	Township	Range	Dir Section	Subsection
CROMWELL 4	49	20	W 33	CABABA

Elevation 1329 **Elev. Method** 7.5 minute topographic map (+/- 5 feet)

Address

Contact: P.O. BOX 74 CROMWELL MN 55726
Well: CROMWELL MN 55726

Stratigraphy Information

Geological Material	From	To (ft.)	Color	Hardness
CLAY	0	5	BROWN	MEDIUM
SAND	5	40	BROWN	SOFT
CLAY	40	80	BROWN	MEDIUM
CLAY	80	175	GRAY	HARD
SAND/GRAVEL	175	200	GRAY	MEDIUM
SAND	200	240	GRAY	SOFT
SAND/GRAVEL	240	250	GRY/BLK	MEDIUM

Remarks

DRILLING METHOD: STAR DRILL.
LOCATION: VILLA VISTA CIRCLE

Well Depth	Depth Completed	Date Well Completed
250 ft.	230 ft.	04/16/1999

Drill Method: Cable Tool   Drill Fluid: Bentonite

Use: community supply(municipal)   Status: Active

Well Hydrofractured? Yes ☐ No ☐ From To

Casing Type: Single casing   Joint: Welded
Drive Shoe? Yes ☒ No ☐ Above/Below

Casing Diameter / **Weight** / **Hole Diameter**
8 in. To 210 ft. 28.5 lbs./ft.   14 in. To 230 ft.

Open Hole From ft. To ft.

Screen? ☒ Type: stainless   Make: JOHNSON

Diameter	Slot/Gauze	Length	Set	
8 in.	50	22 ft.	210 ft.	230 ft.

Static Water Level
21.2 ft. land surface   Measure 04/16/1999

Pumping Level (below land surface)
23.5 ft. 5 hrs. Pumping at 310 g.p.m.

Wellhead Completion
Pitless adapter manufacturer   Model
☒ Casing Protection   ☒ 12 in. above grade
☐ At-grade (Environmental Wells and Borings ONLY)

Grouting Information   Well Grouted? ☒ Yes ☐ No ☐ Not Specified

Material	Amount	From	To
neat cement	70 Sacks	0 ft.	180 ft.

Nearest Known Source of Contamination
feet   Direction   Type
Well disinfected upon completion? ☐ Yes ☐ No

Pump ☐ Not Installed   Date Installed 05/00/1999
Manufacturer's name: GRUNDFOS
Model Number: 150S75-4   HP 7.5   Volt 230
Length of drop pipe 60 ft   Capacity 150 g.p.   Typ Submersible

Abandoned
Does property have any not in use and not sealed well(s)? ☐ Yes ☒ No

Variance
Was a variance granted from the MDH for this well? ☐ Yes ☒ No

Miscellaneous
First Bedrock   Aquifer: Quat. buried
Last Strat: sand +larger   Depth to Bedrock ft
Located by: Minnesota Department of Health
Locate Method: Digitization (Screen) - Map (1:24,000)
System: UTM - NAD83, Zone 15, Meters   X 508617   Y 5170337
Unique Number Verification   Input Date 08/09/2000

Angled Drill Hole

Well Contractor

Licensee Business	Lic. or Reg. No.	Name of Driller
Renner E.H. Well	71015	PRAUGHT, V.

Minnesota Well Index Report   593593   Printed on 05/19/2017 HE-01205-15

Figure 46. Well and Boring Report - Well 519761

Minnesota Unique Well Number

519761

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH

WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

Entry Date 03/04/1993
Update Date 03/10/2014
Received Date

Well Name	Township	Range	Dir Section	Subsection
CROMWELL 3	49	20	W 33	CABAAB

Elevation 1325 **Elev. Method** Calc from DEM (USGS 7.5 min or equiv.)

Address

Contact P.O. BOX 74 CROMWELL MN 55726

Well CROMWELL MN 55726

Stratigraphy Information

Geological Material	From	To (ft.)	Color	Hardness
SANDY CLAY	0	12	BROWN	MEDIUM
SAND WITH CLAY	12	30	BROWN	MEDIUM
SAND	30	55	BROWN	SOFT
FINE SAND	55	62	BROWN	SOFT
FINE SAND & ROCKS	62	90	BROWN	HARD
COARSE SAND	90	92	BROWN	SOFT
CEMENTED SAND &	92	112	BROWN	HARD
CEMENTED SAND &	112	132	BROWN	MEDIUM
CEMENTED SAND &	132	172	BROWN	MED-HRD
MIXED SAND	172	180	BROWN	SOFT
COARSE SAND	180	190	BROWN	SOFT

Remarks

Well Depth	Depth Completed	Date Well Completed
190 ft.	190 ft.	10/21/1992

Drill Method Non-specified Rotary **Drill Fluid** Bentonite

Use community supply(municipal) **Status** Active

Well Hydrofractured? Yes ☐ No ☐ From To

Casing Type Single casing **Joint** Welded

Drive Shoe? Yes ☒ No ☐ **Above/Below** 0 ft.

Casing Diameter **Weight** **Hole Diameter**
8 in. To 180 ft. 28.5 lbs./ft. 10 in. To 190 ft.

Open Hole From ft. To ft.

Screen? ☒ **Type** stainless **Make** COOK

Diameter	Slot/Gauze	Length	Set	
8 in.	25	10 ft.	180 ft.	190 ft.

Static Water Level
16 ft. land surface **Measure** 10/20/1992

Pumping Level (below land surface)
32.1 ft. 24 hrs. Pumping at 290 g.p.m.

Wellhead Completion
Pitless adapter manufacturer Model
☐ Casing Protection ☒ 12 in. above grade
☐ At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? ☒ Yes ☐ No ☐ Not Specified

Material	Amount	From	To
bentonite	0	0 ft.	180 ft.

Nearest Known Source of Contamination
100 feet Southeas Direction Septic tank/drain field Type
Well disinfected upon completion? ☐ Yes ☐ No

Pump ☒ Not Installed Date Installed
Manufacturer's name
Model Number HP 0 Volt
Length of drop pipe ft Capacity g.p. Typ

Abandoned
Does property have any not in use and not sealed well(s)? ☐ Yes ☒ No

Variance
Was a variance granted from the MDH for this well? ☐ Yes ☐ No

Miscellaneous
First Bedrock Aquifer Quat. buried
Last Strat sand-brown Depth to Bedrock ft
Located by Minnesota Department of Health
Locate Method Digitization (Screen) - Map (1:24,000)
System UTM - NAD83, Zone 15, Meters X 508644 Y 5170337
Unique Number Verification Information from Input Date 10/18/1999

Angled Drill Hole

Well Contractor

Peterson Well Co.	69183	PETERSEN, D.
Licensee Business	Lic. or Reg. No.	Name of Driller

Minnesota Well Index Report **519761**

Printed on 05/19/2017
HE-01205-15

Figure 47. Well and Boring Report - Well 773071

Minnesota Unique Well Number: 773071
County: Carlton
Quad: Cromwell
Quad ID: 226B

MINNESOTA DEPARTMENT OF HEALTH
WELL AND BORING REPORT
Minnesota Statutes Chapter 1031

Entry Date: 08/14/2015
Update Date: 10/21/2015
Received Date:

Well Name	Township	Range	Dir	Section	Subsection
CWO1-A	49	20	W	33	CABADB

Elevation: 1325.9 Elev. Method: LiDAR 1m DEM (MNDNR)

Address
Contact: 1220 VILLA COURT DR CROMWELL MN 55726
Well: 1189 VILLA VISTA CI CROMWELL MN 55726

Stratigraphy Info: [illegible]OODALE DR MOUNDS VIEW MN 55112

Geological Material	From	To (ft.)	Color	Hardness
GRAVEL WITH SAND &	0	8	BRN/RED	SOFT
SILT, SAND & CLAY W/	8	11	RED/BRN	MEDIUM
GRAVEL & SAND WITH	11	22	GRAY	MEDIUM
SAND & GRAVEL WITH	22	43	GRAY	MEDIUM
SAND WITH SILT &	43	101	RED/BRN	MEDIUM
SILT SAND CLAY	101	150	VARIED	MED-HRD

Remarks:
SEE DRILLERS LOG FOR DETAILED INFORMATION.
GAMMA & EM INDUCTION LOGGED 8-13-2015. LOGGED FOR USGS.

Well Depth: 150 ft. Depth Completed: 147.97 ft. Date Well Completed: 07/21/2015
Drill Method: Non-specified Rotary Drill Fluid: Bentonite
Use: environ. bore hole Status: Active
Well Hydrofractured? Yes [ ] No [X] From To
Casing Type: Single casing Joint
Drive Shoe? Yes [ ] No [X] Above/Below

Casing Diameter	Weight	Hole Diameter
2 in. To 144. ft.	0.68 lbs./ft.	6.7 in. To 150 ft.

Open Hole From ft. To ft.
Screen? [X] Type: slotted pipe Make: JOHNSON

Diameter	Slot/Gauze	Length	Set
2 in.	10	2.8 ft.	144.5 ft. 147.3 ft.

Static Water Level
20.1 ft. land surface Measure 08/17/2015

Pumping Level (below land surface)
ft. 6.0 hrs. Pumping at 0.79 g.p.m.

Wellhead Completion
Pitless adapter manufacturer: Model:
[X] Casing Protection [X] 12 in. above grade
[ ] At-grade (Environmental Wells and Borings ONLY)

Grouting Information: Well Grouted? [X] Yes [ ] No [ ] Not Specified

Material	Amount	From	To
bentonite	12 Sacks	2 ft.	144 ft.
concrete	3 Sacks	ft.	2 ft.

Nearest Known Source of Contamination
foot Direction Type
Well disinfected upon completion? [ ] Yes [X] No

Pump [X] Not Installed Date Installed
Manufacturer's name
Model Number HP Volt
Length of drop pipe ft Capacity g.p. Typ

Abandoned
Does property have any not in use and not sealed well(s)? [ ] Yes [X] No

Variance
Was a variance granted from the MDH for this well? [ ] Yes [X] No

Miscellaneous:
First Bedrock Aquifer Quat. buried
Last Strat pebbly sand/silt/clay Depth to Bedrock ft
Located by Minnesota Geological Survey
Locate Method Digitization (Screen) - Map (1:24,000)
System UTM - NAD83, Zone 15, Meters X 508636 Y 5170295
Unique Number Verification Information from Input Date 08/14/2015

Angled Drill Hole

Well Contractor
US Geological Survey 1548 LEININGER, R.
Licensee Business Lic. or Reg. No. Name of Driller

Minnesota Well Index Report | 773071 | Printed on 05/19/2017
HE-01205-15

Figure 48. Well and Boring Report - Well 773070

Minnesota Unique Well Number

773070

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH

WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

Entry Date 08/14/2015
Update Date 10/21/2015
Received Date

Well Name	Township	Range	Dir Section	Subsection
CWO1-B	49	20	W 33	CABADB

Elevation 1325.8 **Elev. Method** LiDAR 1m DEM (MNDNR)

Address

Contact 1220 VILLA COURT DRIVE CROMWELL MN 55726
Well 1189 VILLA VISTA CI CROMWELL MN 55726
2280 WOODALE DR MOUNDS VIEW MN 55112

Stratigraphy Information

Geological Material	From	To (ft.)	Color	Hardness
GRAVEL WITH SAND &	0	8	BRN/RED	SOFT
SILT, SAND & CLAY	8	11	RED/BRN	MEDIUM
GRAVEL & SAND WITH	11	22	GRAY	MEDIUM
SAND & GRAVEL WITH	22	43	GRAY	MEDIUM
SAND WTH SILT AND	43	101	RED/BRN	MEDIUM
SILT, SAND, CLAY	101	173	VARIED	MED-HRD
SAND & GRAVEL	173	231	VARIED	MED-HRD

Well Depth 230.9 ft. **Depth Completed** 230.87 ft. **Date Well Completed** 07/20/2015

Drill Method Non-specified Rotary **Drill Fluid** Bentonite

Use monitor well **Status** Active

Well Hydrofractured? Yes ☐ No ☒ **From** **To**

Casing Type Single casing **Joint**

Drive Shoe? Yes ☐ No ☒ **Above/Below**

Casing Diameter **Weight** **Hole Diameter**
2 in. To 220. ft. 0.68 lbs./ft. 6.7 in. To 23.5 ft.

Open Hole From ft. To ft.

Screen? ☒ **Type** slotted pipe **Make** ENVIRONMENTAL

Diameter	Slot/Gauze	Length	Set	
2 in.	20	9.6 ft.	220.9 ft.	230.5 ft.

Static Water Level
16.7 ft. land surface **Measure** 08/17/2015

Pumping Level (below land surface)
ft. 3.9 hrs. Pumping at 1.35 g.p.m.

Wellhead Completion
Pitless adapter manufacturer Model
☒ Casing Protection ☒ 12 in. above grade
☐ At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? ☒ Yes ☐ No ☐ Not Specified

Material	Amount	From	To
bentonite	12 Sacks	2 ft.	215.7 ft.
concrete	3 Sacks	ft.	2 ft.

Nearest Known Source of Contamination
feet Direction Type
Well disinfected upon completion? ☐ Yes ☒ No

Pump ☒ Not Installed Date Installed
Manufacturer's name
Model Number HP Volt
Length of drop pipe ft Capacity g.p. Typ

Abandoned
Does property have any not in use and not sealed well(s)? ☐ Yes ☒ No

Variance
Was a variance granted from the MDH for this well? ☐ Yes ☒ No

Miscellaneous
First Bedrock Aquifer Quat. buried
Last Strat pebbly sand/silt/clay Depth to Bedrock ft
Located by Minnesota Geological Survey
Locate Method Digitization (Screen) - Map (1:24,000)
System UTM - NAD83, Zone 15, Meters X 508635 Y 5170295
Unique Number Verification Information from Input Date 08/14/2015

Remarks
SEE DRILLERS LOG FOR DETAILED INFORMATION.
GAMMA & EM INDUCTION LOGGED 8-13-2015. LOGGED FOR USGS.

Angled Drill Hole

Well Contractor

Licensee Business	Lic. or Reg. No.	Name of Driller
US Geological Survey	1548	LEININGER, R.

Minnesota Well Index Report 773070

Printed on 05/19/2017
HE-01205-15

Figure 49. Well and Boring Report - Well 773069

Minnesota Unique Well Number **773069**

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH
WELL AND BORING REPORT
Minnesota Statutes Chapter 1031

Entry Date 08/14/2015
Update Date 10/21/2015
Received Date

Well Name	Township	Range	Dir Section	Subsection
CWO1-C	49	20	W 33	CABADB

Elevation 1325.8 **Elev. Method** LiDAR 1m DEM (MNDNR)

Address
Contact 1220 VILLA COURT DRIVE CROMWELL MN 55726
Well 1189 VILLA VISTA CI CROMWELL MN 55726

Stratigraphy Information …ODALE DR MOUNDS VIEW MN 55112

Geological Material	From	To (ft.)	Color	Hardness
GRAVEL WITH SAND	0	8	BRN/RED	SOFT
SILT, SAND & CLAY	8	11	RED/BRN	MEDIUM
GRAVEL & SAND W	11	22	GRAY	MEDIUM
SAND & GRAVEL WITH	22	43	GRAY	MEDIUM
SILT, SAND, CLAY	43	173	RED/BRN	HARD
SAND & GRAVEL	173	320	VARIED	MED-HRD
CLAY WITH SLATE	320	342	BLU/GRY	HARD

Remarks
SEE DRILLER LOG FOR DETAILED INFORMATION.
GAMMA & EM INDUCTION LOGGED 8-13-2015. LOGGED FOR USGS.

Well Depth 342 ft. **Depth Completed** 339.59 ft. **Date Well Completed** 07/18/2015
Drill Method Non-specified Rotary **Drill Fluid** Bentonite

Use environ. bore hole **Status** Active

Well Hydrofractured? Yes ☐ No ☒ From To

Casing Type Single casing **Joint**
Drive Shoe? Yes ☐ No ☒ Above/Below

Casing Diameter **Weight** **Hole Diameter**
2 in. To 330 ft. 0.68 lbs./ft. 6.7 in. To 340 ft.

Open Hole From ft. To ft.
Screen? ☒ **Type** slotted pipe **Make** ENVIRONMENTAL
Diameter Slot/Gauze Length Set
2 in. 20 9.6 ft. 329.9 ft. 339.5 ft.

Static Water Level
16.7 ft. land surface **Measure** 08/17/2015

Pumping Level (below land surface)
ft. 3.9 hrs. Pumping at 1.48 g.p.m.

Wellhead Completion
Pitless adapter manufacturer Model
☒ Casing Protection ☒ 12 in. above grade
☐ At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? ☒ Yes ☐ No ☐ Not Specified

Material	Amount		From	To
bentonite	28	Sacks	2 ft.	324 ft.
concrete	3	Sacks	ft.	2 ft.

Nearest Known Source of Contamination
feet Direction Type
Well disinfected upon completion? ☐ Yes ☒ No

Pump ☒ Not Installed Date Installed
Manufacturer's name
Model Number HP Volt
Length of drop pipe ft Capacity g.p. Typ

Abandoned
Does property have any not in use and not sealed well(s)? ☐ Yes ☒ No

Variance
Was a variance granted from the MDH for this well? ☐ Yes ☒ No

Miscellaneous
First Bedrock **Aquifer** Quat. buried
Last Strat pebbly sand/silt/clay-gray Depth to Bedrock ft
Located by Minnesota Geological Survey
Locate Method Digitization (Screen) - Map (1:24,000)
System UTM - NAD83, Zone 15, Meters X 508633 Y 5170295
Unique Number Verification Information from Input Date 08/14/2015

Angled Drill Hole

Well Contractor
US Geological Survey 1548 LEININGER, R.
Licensee Business Lic. or Reg. No. Name of Driller

Minnesota Well Index Report 773069 Printed on 05/19/2017 HE-01205-15

Figure 50. Well and Boring Report - Well 773068

Minnesota Unique Well Number

773068

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH

WELL AND BORING REPORT

Minnesota Statutes Chapter 1031

Entry Date 08/14/2015
Update Date 10/20/2015
Received Date

Well Name	Township	Range	Dir Section	Subsection
CWO2-A	49	20	W 33	CABABA

Elevation 1332 **Elev. Method** LiDAR 1m DEM (MNDNR)

Address

Well 1189 VILLA VISTA CI CROMWELL MN 55726

C/W 2280 WOODALE DR MOUNDS VIEW MN 55112

Stratigraphy Information CROMWELL MN 55726

Geological Material	From	To (ft.)	Color	Hardness
COARSE SAND &	0	8	RED/BRN	SOFT
SILTY SANDY CLAY	8	11	RED/BRN	HARD
SAND & GRAVEL	11	22	GRAY	HARD
SAND & GRAVEL	22	43	GRAY	HARD
CLAY W/SILT & SAND,	43	120	RED/BRN	HARD
SAND, SILTY WITH	120	174	BROWN	HARD

Remarks

SEE DRILLERS LOG FOR DETAILED INFORMATION.

Well Depth 174 ft. **Depth Completed** 35.17 ft. **Date Well Completed** 07/09/2015

Drill Method Auger (non-specified) **Drill Fluid**

Use environ. bore hole **Status** Active

Well Hydrofractured? Yes ☐ No ☒ From To

Casing Type Single casing **Joint**

Drive Shoe? Yes ☐ No ☐ **Above/Below**

Casing Diameter **Weight** **Hole Diameter**

1.2 in. To 34.8 ft. 0.74 lbs./ft. 8.2 in. To 174 ft.

Open Hole From ft. To ft.

Screen? ☒ Type slotted pipe **Make** ENVIRONMENTAL

Diameter	Slot/Gauze	Length	Set	
1.2 in.	10	2.7 ft.	32.5 ft.	35.1 ft.

Static Water Level

28.6 ft. land surface **Measure** 08/17/2015

Pumping Level (below land surface)

ft. 2.8 hrs. Pumping at 0.17 g.p.m.

Wellhead Completion

Pitless adapter manufacturer Model

☒ Casing Protection ☒ 12 in. above grade

☐ At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? ☒ Yes ☐ No ☐ Not Specified

Material Amount From To

well grouted, type unknown ft. ft.

Nearest Known Source of Contamination

feet Direction Type

Well disinfected upon completion? ☐ Yes ☒ No

Pump ☒ Not Installed Date Installed

Manufacturer's name

Model Number HP Volt

Length of drop pipe ft Capacity g.p. Typ

Abandoned

Does property have any not in use and not sealed well(s)? ☐ Yes ☒ No

Variance

Was a variance granted from the MDH for this well? ☐ Yes ☒ No

Miscellaneous

First Bedrock Aquifer Quat. buried

Last Strat sand+silt-brown Depth to Bedrock ft

Located by Minnesota Geological Survey

Locate Method Digitization (Screen) - Map (1:24,000)

System UTM - NAD83, Zone 15, Meters X 508625 Y 5170347

Unique Number Verification Information from Input Date 08/14/2015

Angled Drill Hole

Well Contractor

US Geological Survey	1548	HUCKABY, J.
Licensee Business	Lic. or Reg. No.	Name of Driller

Minnesota Well Index Report 773068

Printed on 05/22/2017

HE-01205-15

Figure 51. Well and Boring Report - Well 773067

Minnesota Unique Well Number

773067

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH
WELL AND BORING REPORT
Minnesota Statutes Chapter 1031

Entry Date 08/14/2015
Update Date 10/20/2015
Received Date

Well Name	Township	Range	Dir Section	Subsection
CWO2-B	49	20	W 33	CABABA

Elevation 1332.2 **Elev. Method** LiDAR 1m DEM (MNDNR)

Address
Well 1189 VILLA VISTA CI CROMWELL MN 55726
Contact 2280 WOODALE DR CROMWELL MN 55112

Stratigraphy Information CROMWELL MN 55726

Geological Material	From	To (ft.)	Color	Hardness
COARSE SAND &	0	8	RED/BRN	SOFT
SAND, SILTY WITH	8	11	RED/BRN	MEDIUM
GRAVEL & SAND,	11	22	DK. GRY	MEDIUM
SAND WITH SILT, MED.	22	40	DK. GRY	MEDIUM
SAND&GRVL POOR	40	43	DK. GRY	HARD
SILTY CLAY	43	61	RED/BRN	HARD

Remarks
SEE DRILLERS LOG FOR DETAILED INFORMATION.

Well Depth	Depth Completed	Date Well Completed
60.5 ft.	59.62 ft.	07/13/2015

Drill Method Auger (non-specified) **Drill Fluid**

Use environ. bore hole **Status** Active

Well Hydrofractured? Yes ☐ No ☒ From To

Casing Type Single casing **Joint**
Drive Shoe? Yes ☐ No ☐ Above/Below

Casing Diameter **Weight** **Hole Diameter**
1.2 in. To 56.8 ft. 0.74 lbs./ft. 8.2 in. To 60.5 ft.

Open Hole From ft. To ft.
Screen? ☒ **Type** slotted pipe **Make** ENVIRONMENTAL

Diameter	Slot/Gauze	Length	Set	
1.2 in.	10	2.7 ft.	57 ft.	59.6 ft.

Static Water Level
27.9 ft. land surface **Measure** 08/18/2015

Pumping Level (below land surface)
ft. 2.1 hrs. Pumping at 0.15 g.p.m.

Wellhead Completion
Pitless adapter manufacturer Model
☒ Casing Protection ☐ 12 in. above grade
☐ At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? ☒ Yes ☐ No ☐ Not Specified

Material	Amount		From	To
bentonite	6	Sacks	2 ft.	55 ft.
concrete	1	Sacks	ft.	2 ft.

Nearest Known Source of Contamination
feet Direction Type
Well disinfected upon completion? ☐ Yes ☒ No

Pump ☒ Not Installed Date Installed
Manufacturer's name
Model Number HP Volt
Length of drop pipe ft Capacity g.p. Typ

Abandoned
Does property have any not in use and not sealed well(s)? ☐ Yes ☒ No

Variance
Was a variance granted from the MDH for this well? ☐ Yes ☒ No

Miscellaneous
First Bedrock Aquifer Quat. buried
Last Strat pebbly sand/silt/clay Depth to Bedrock ft
Located by Minnesota Geological Survey
Locate Method Digitization (Screen) - Map (1:24,000)
System UTM - NAD83, Zone 15, Meters X 508625 Y 5170349
Unique Number Verification Information from Input Date 08/14/2015

Angled Drill Hole

Well Contractor

Licensee Business	Lic. or Reg. No.	Name of Driller
US Geological Survey	1548	HUCKABY, J.

Minnesota Well Index Report 773067

Printed on 05/22/2017
HE-01205-15

Figure 52. Well and Boring Report - Well 773066

Minnesota Unique Well Number

773066

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH
WELL AND BORING REPORT
Minnesota Statutes Chapter 1031

Entry Date 08/14/2015
Update Date 10/20/2015
Received Date

Well Name	Township	Range	Dir Section	Subsection
CWO2-C	49	20	W 33	CABAAB

Elevation 1331.9 **Elev. Method** LiDAR 1m DEM (MNDNR)

Address
Well 1189 VILLA VISTA CI CROMWELL MN 55726
Contact 2280 WOODALE DR MOUNDS VIEW MN 55112

Stratigraphy Information CROMWELL MN 55726

Geological Material	From	To (ft.)	Color	Hardness
COARSE SAND &	0	8	RED/BRN	SOFT
SAND, SILTY WITH	8	11	RED/BRN	MEDIUM
GRAVEL & SAND,	11	22	DK. GRY	MEDIUM
SAND WITH SILT, MED.	22	40	DK. GRY	MEDIUM
SAND&GRVL, POOR	40	82	DK. GRY	HARD

Remarks
SEE DRILLERS LOG FOR DETAILED INFORMATION.

Well Depth	Depth Completed	Date Well Completed
81.57 ft.	81.57 ft.	07/10/2015

Drill Method Auger (non-specified) **Drill Fluid**

Use environ. bore hole **Status** Active

Well Hydrofractured? Yes [ ] No [X] **From** **To**

Casing Type Single casing **Joint**
Drive Shoe? Yes [ ] No [ ] **Above/Below**

Casing Diameter **Weight** **Hole Diameter**
1.2 in. To 78.7 ft. 0.74 lbs./ft. 8.2 in. To 81.5 ft.

Open Hole From ft. To ft.
Screen? [X] **Type** slotted pipe **Make** ENVIRONMENTAL

Diameter	Slot/Gauze	Length	Set	
1.2 in.	10	2.7 ft.	79.9 ft.	81.5 ft.

Static Water Level
26.5 ft. land surface **Measure** 08/18/2015

Pumping Level (below land surface)
ft. 12. hrs. Pumping at 0.3 g.p.m.

Wellhead Completion
Pitless adapter manufacturer **Model**
[X] Casing Protection [X] 12 in. above grade
[ ] At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? [X] Yes [ ] No [ ] Not Specified

Material	Amount		From	To
bentonite	6	Sacks	2 ft.	73.5 ft.
concrete	1.5	Sacks	ft.	2 ft.

Nearest Known Source of Contamination
feet Direction Type
Well disinfected upon completion? [ ] Yes [X] No

Pump [X] Not Installed Date Installed
Manufacturer's name
Model Number HP Volt
Length of drop pipe ft Capacity g.p. Typ

Abandoned
Does property have any not in use and not sealed well(s)? [ ] Yes [X] No

Variance
Was a variance granted from the MDH for this well? [ ] Yes [X] No

Miscellaneous
First Bedrock Aquifer Quat. Water
Last Strat sand+silt-gray Depth to Bedrock ft
Located by Minnesota Geological Survey
Locate Method Digitization (Screen) - Map (1:24,000)
System UTM - NAD83, Zone 15, Meters X 508627 Y 5170347
Unique Number Verification Information from Input Date 08/14/2015

Angled Drill Hole

Well Contractor

Licensee Business	Lic. or Reg. No.	Name of Driller
US Geological Survey	1548	HUCKABY, J.

Minnesota Well Index Report 773066

Printed on 05/22/2017
HE-01205-15

Figure 53. Well and Boring Report - Well 773065

Minnesota Unique Well Number

773065

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH
WELL AND BORING REPORT
Minnesota Statutes Chapter 1031

Entry Date 08/14/2015
Update Date 10/23/2015
Received Date

Well Name	Township	Range	Dir Section	Subsection
CWO2-D	49	20	W 33	CABABA

Elevation 1331.9 **Elev. Method** LiDAR 1m DEM (MNDNR)

Address

Well 1189 VILLA VISTA CI CROMWELL MN 55726

Contact 2280 WOODALE DR MOUNDS VIEW MN 55112

Stratigraphy Information / CROMWELL MN 55726

Geological Material	From	To (ft.)	Color	Hardness
COARSE SAND &	0	8	RED/BRN	SOFT
SAND, SILTY W/CLAY	8	11	RED/BRN	MEDIUM
COARSE SAND &	11	22	DK. GRY	MEDIUM
SAND W/ SILT, MED.	22	40	DK. GRY	MEDIUM
SAND&GRVL POOR	40	43	DK. GRY	HARD
SILTY CLAY	43	108	RED/BRN	HARD

Remarks

SEE DRILLERS LOG FOR DETAILED INFORMATION.

CORE TAKEN FROM O FT. TO 107 FT. AS PART OF USGS TILL STUDY.

Well Depth	Depth Completed	Date Well Completed
107.5 ft.	106.45 ft.	06/29/2015

Drill Method Auger (non-specified) **Drill Fluid**

Use environ. bore hole **Status** Active

Well Hydrofractured? Yes [ ] No [X] From To

Casing Type Single casing **Joint**
Drive Shoe? Yes [ ] No [ ] Above/Below

Casing Diameter **Weight** **Hole Diameter**
1.2 in. To 103. ft. 0.74 lbs./ft. 8.2 in. To 107. ft.

Open Hole From ft. To ft.

Screen? [X] **Type** slotted pipe **Make** ENVIRONMENTAL

Diameter	Slot/Gauze	Length	Set	
1.2 in.	10	2.7 ft.	103.8 ft.	106.4 ft.

Static Water Level
23.4 ft. land surface **Measure** 08/18/2015

Pumping Level (below land surface)
ft. 1.1 hrs. Pumping at 0.33 g.p.m.

Wellhead Completion
Pitless adapter manufacturer Model
[X] Casing Protection [ ] 12 in. above grade
[ ] At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? [X] Yes [ ] No [ ] Not Specified

Material	Amount		From	To
bentonite	9	Sacks	2.5 ft.	92 ft.
concrete	2	Sacks	ft.	2.5 ft.

Nearest Known Source of Contamination
feet Direction Type
Well disinfected upon completion? [ ] Yes [X] No

Pump [X] Not Installed Date Installed
Manufacturer's name
Model Number HP Volt
Length of drop pipe ft Capacity g.p. Typ

Abandoned
Does property have any not in use and not sealed well(s)? [ ] Yes [X] No

Variance
Was a variance granted from the MDH for this well? [ ] Yes [X] No

Miscellaneous
First Bedrock Aquifer Quat. buried
Last Strat pebbly sand/silt/clay Depth to Bedrock ft
Located by Minnesota Geological Survey
Locate Method Digitization (Screen) - Map (1:24,000)
System UTM - NAD83, Zone 15, Meters X 508624 Y 5170347
Unique Number Verification Information from Input Date 08/14/2015

Angled Drill Hole

Well Contractor

US Geological Survey	1548	HUCKABY, J.
Licensee Business	Lic. or Reg. No.	Name of Driller

Minnesota Well Index Report 773065

Printed on 05/22/2017
HE-01205-15

Figure 54. Well and Boring Report - Well 773064

Minnesota Unique Well Number

773064

County Carlton
Quad Cromwell
Quad ID 226B

MINNESOTA DEPARTMENT OF HEALTH
WELL AND BORING REPORT
Minnesota Statutes Chapter 1031

Entry Date 08/14/2015
Update Date 10/23/2015
Received Date

Well Name	Township	Range	Dir Section	Subsection
CWO2-E	49	20	W 33	CABABA

Elevation 1331.9 **Elev. Method** LiDAR 1m DEM (MNDNR)

Address

Well 1189 VILLA VISTA CI CROMWELL MN 55726

Contact 2280 WOODALE DR MOUNDS VIEW MN 55112

Stratigraphy Information CROMWELL MN 55726

Geological Material	From	To (ft.)	Color	Hardness
COARSE SAND &	0	8	RED/BRN	SOFT
SAND, SILTY W/CLAY	8	11	RED/BRN	MEDIUM
GRAVEL & SAND	11	22	DK. GRY	MEDIUM
SAND W/SILT MED. TO	22	40	DK. GRY	MEDIUM
SAND & GRVL POOR	40	43	DK. GRY	HARD
SILTY CLAY	43	120	RED/BRN	HARD
SILTY SANDY CLAY	120	130	DK. BRN	HARD

Remarks

SEE DRILLERS LOG FOR DETAILED INFORMATION.

CORE TAKEN FROM 108 FT. TO 120.5 FT. AS PART OF USGS TILL STUDY.

Well Depth	Depth Completed	Date Well Completed
129.5 ft.	128.65 ft.	07/12/2015

Drill Method Auger (non-specified) **Drill Fluid**

Use environ. bore hole **Status** Active

Well Hydrofractured? Yes ☐ No ☐ **From** **To**

Casing Type Single casing **Joint**

Drive Shoe? Yes ☐ No ☐ **Above/Below**

Casing Diameter **Weight** **Hole Diameter**

1.2 in. To 125. ft. 0.74 lbs./ft. 8.2 in. To 129. ft.

Open Hole From ft. To ft.

Screen? ☒ **Type** slotted pipe **Make** ENVIRONMENTAL

Diameter	Slot/Gauze	Length	Set	
1.2 in.	10	2.7 ft.	126 ft.	128.6 ft.

Static Water Level

23.9 ft. land surface **Measure** 08/18/2015

Pumping Level (below land surface)

ft. 3.9 hrs. Pumping at 0.4 g.p.m.

Wellhead Completion

Pitless adapter manufacturer **Model**

☒ Casing Protection ☐ 12 in. above grade

☐ At-grade (Environmental Wells and Borings ONLY)

Grouting Information Well Grouted? ☒ Yes ☐ No ☐ Not Specified

Material	Amount		From	To
bentonite	8	Sacks	2 ft.	24.1 ft.
concrete	2	Sacks	ft.	2 ft.

Nearest Known Source of Contamination

feet Direction Type

Well disinfected upon completion? ☐ Yes ☒ No

Pump ☒ Not Installed **Date Installed**

Manufacturer's name

Model Number HP Volt

Length of drop pipe ft Capacity g.p. Typ

Abandoned

Does property have any not in use and not sealed well(s)? ☐ Yes ☒ No

Variance

Was a variance granted from the MDH for this well? ☐ Yes ☒ No

Miscellaneous

First Bedrock **Aquifer** Quat. buried

Last Strat pebbly sand/silt/clay- Depth to Bedrock ft

Located by Minnesota Geological Survey

Locate Method Digitization (Screen) - Map (1:24,000)

System UTM - NAD83, Zone 15, Meters X 508624 Y 5170349

Unique Number Verification Information from Input Date 08/14/2015

Angled Drill Hole

Well Contractor

Licensee Business	Lic. or Reg. No.	Name of Driller
US Geological Survey	1548	HUCKABY, J.

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